

THE APPLICATION OF POM
TO THE CAVITY
BENEATH THE AMERY ICE SHELF

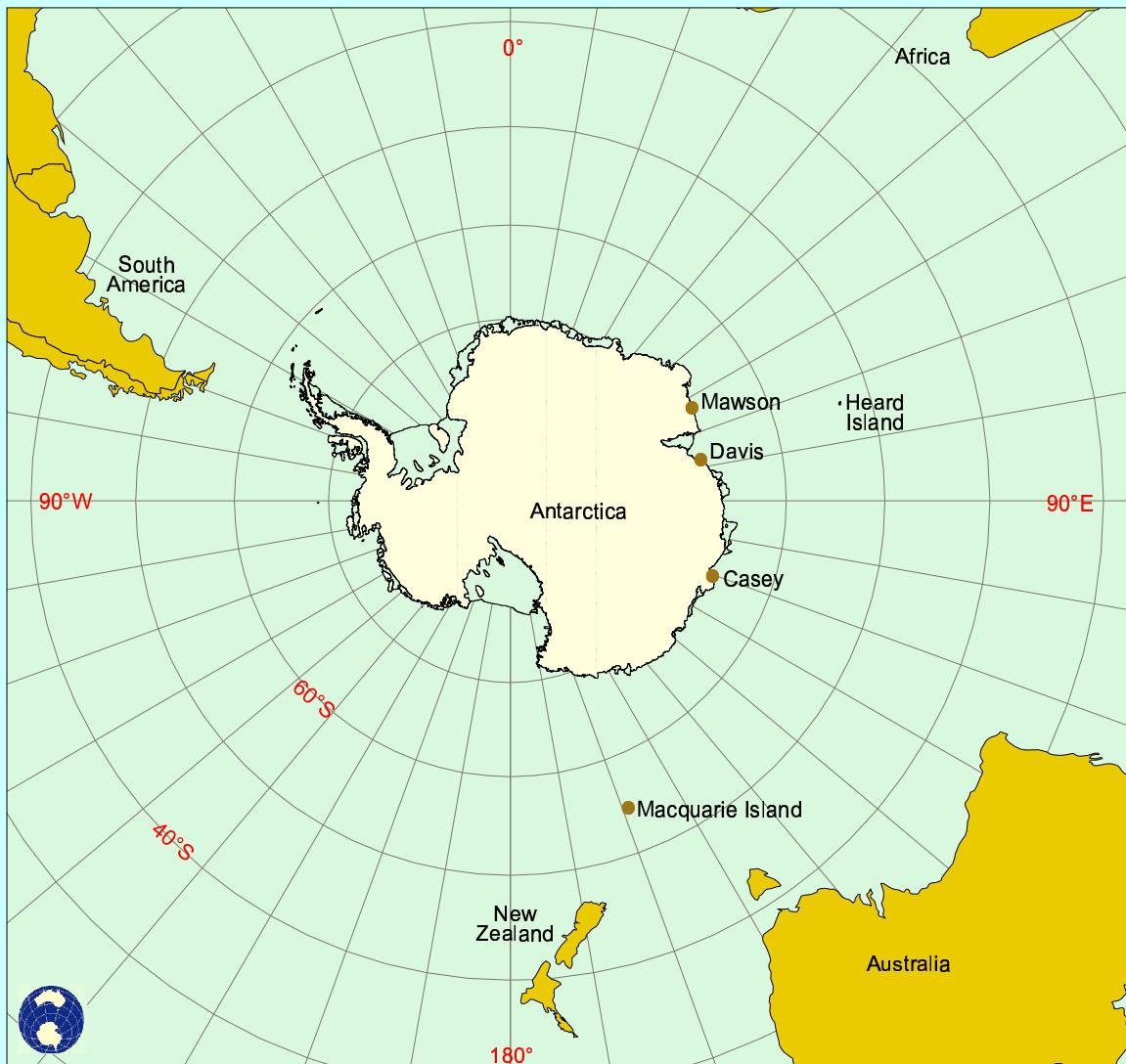
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Antarctica

Permanent Australian Stations

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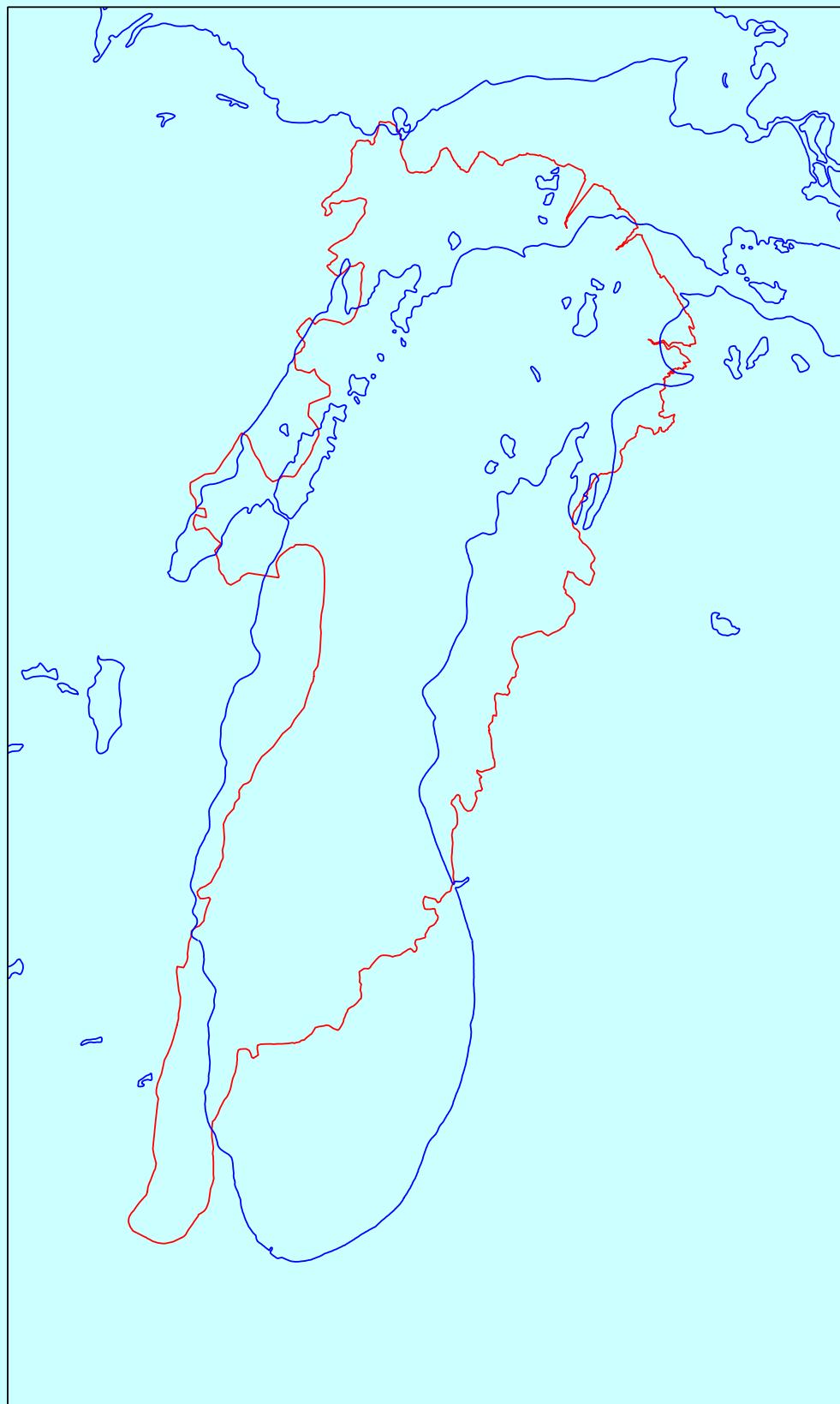
Projection: Polar Stereographic
True Scale at 71°S

● Permanent
Australian
Station

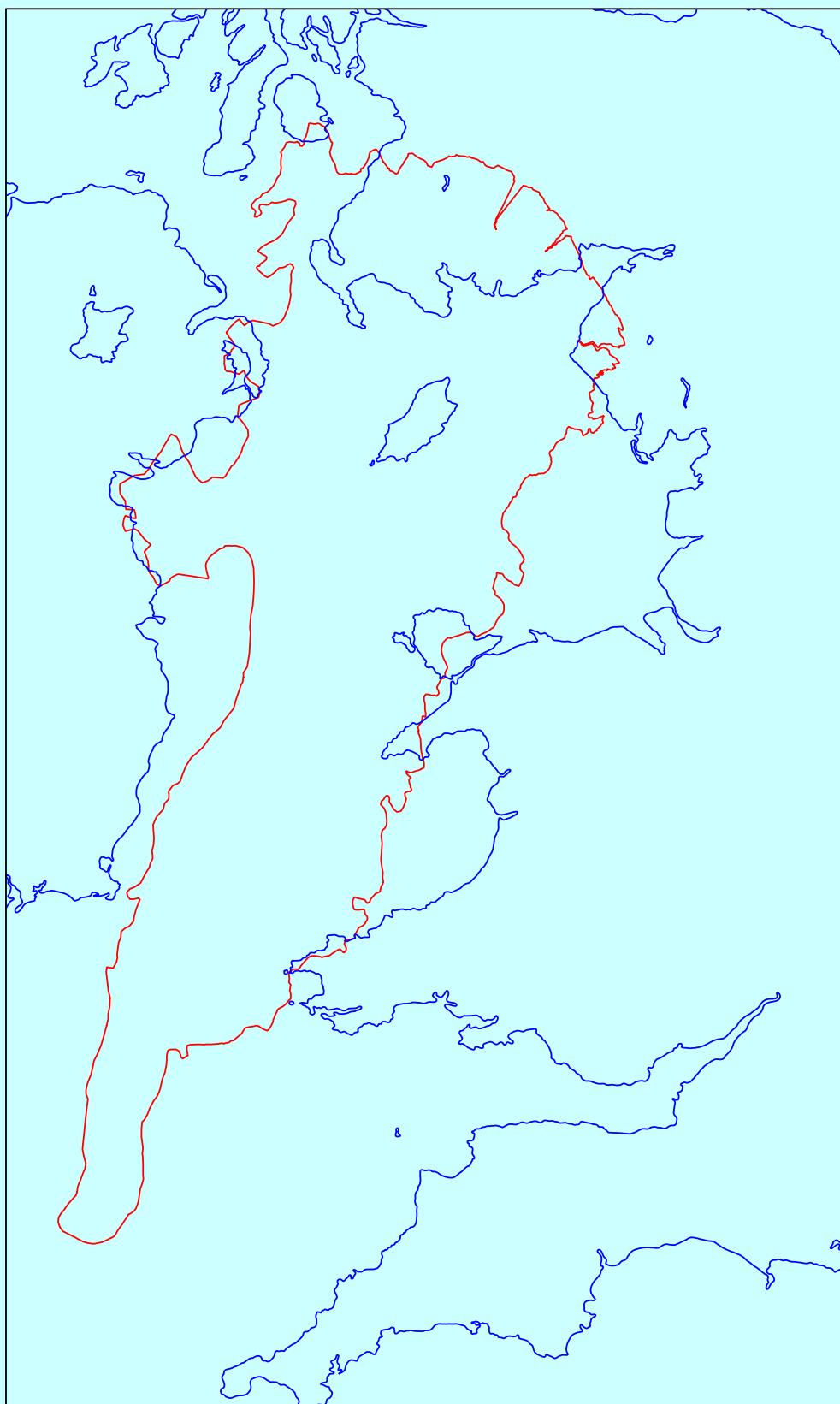
Amery Ice Front



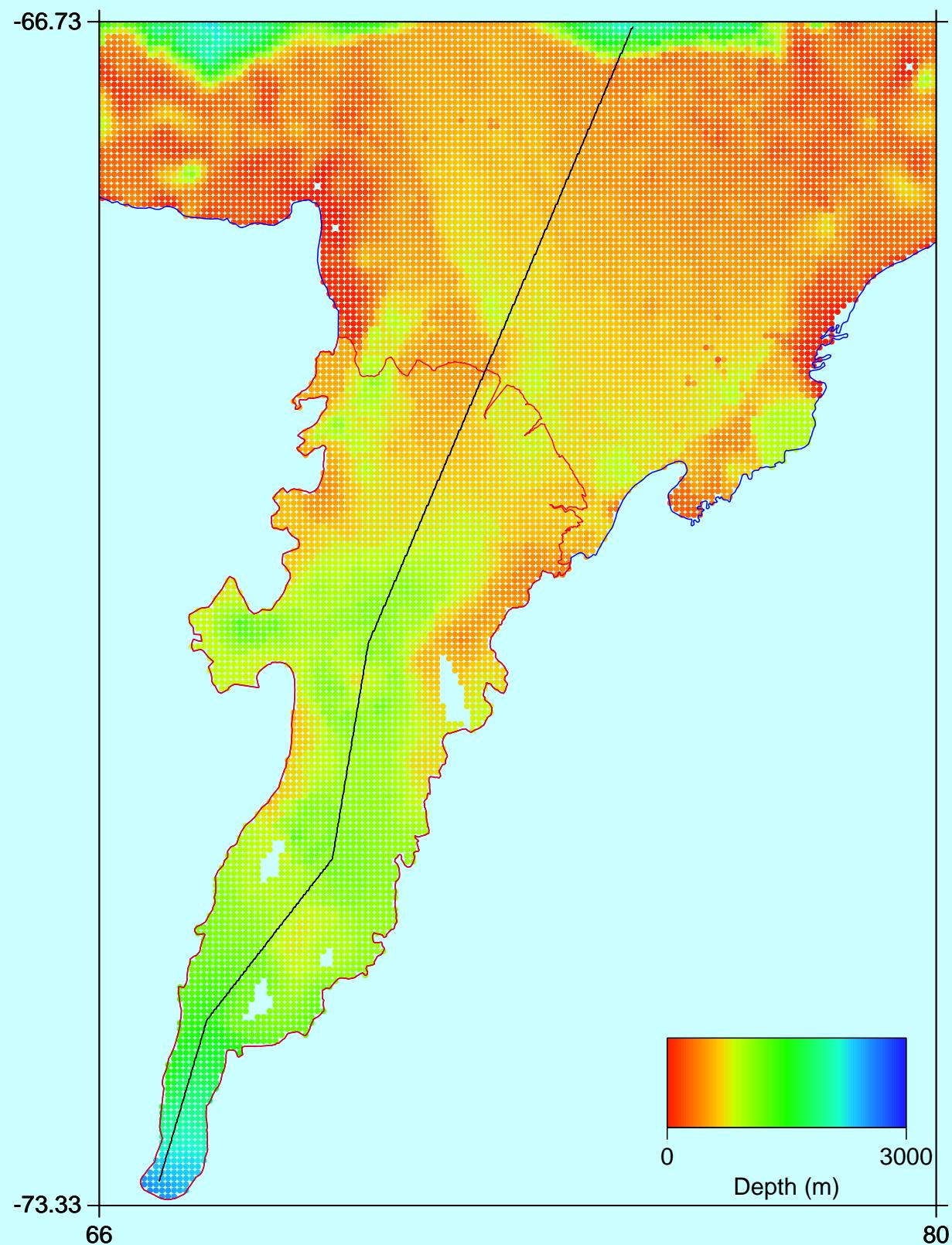
Amery vs Lake Michigan



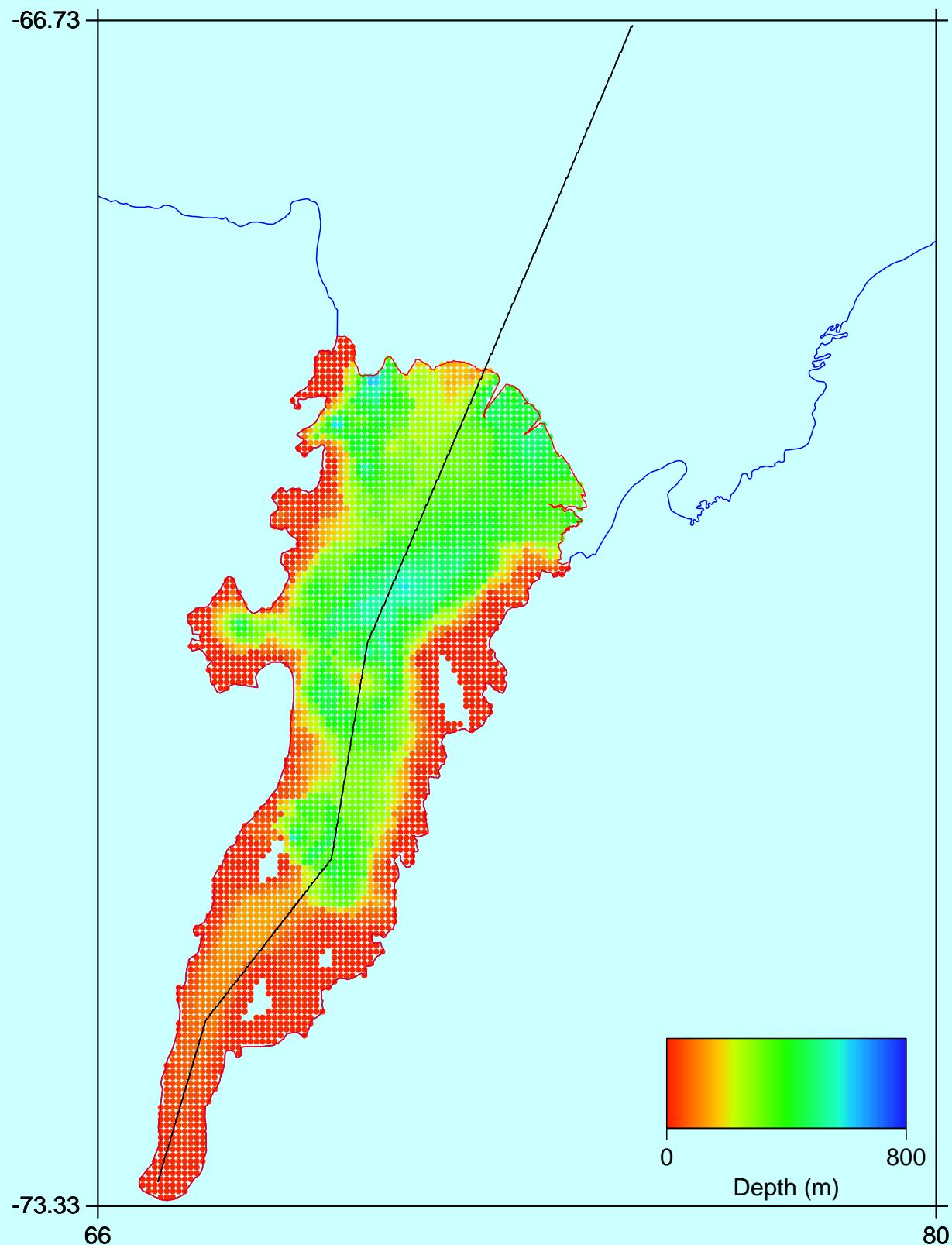
Amery vs Irish Sea



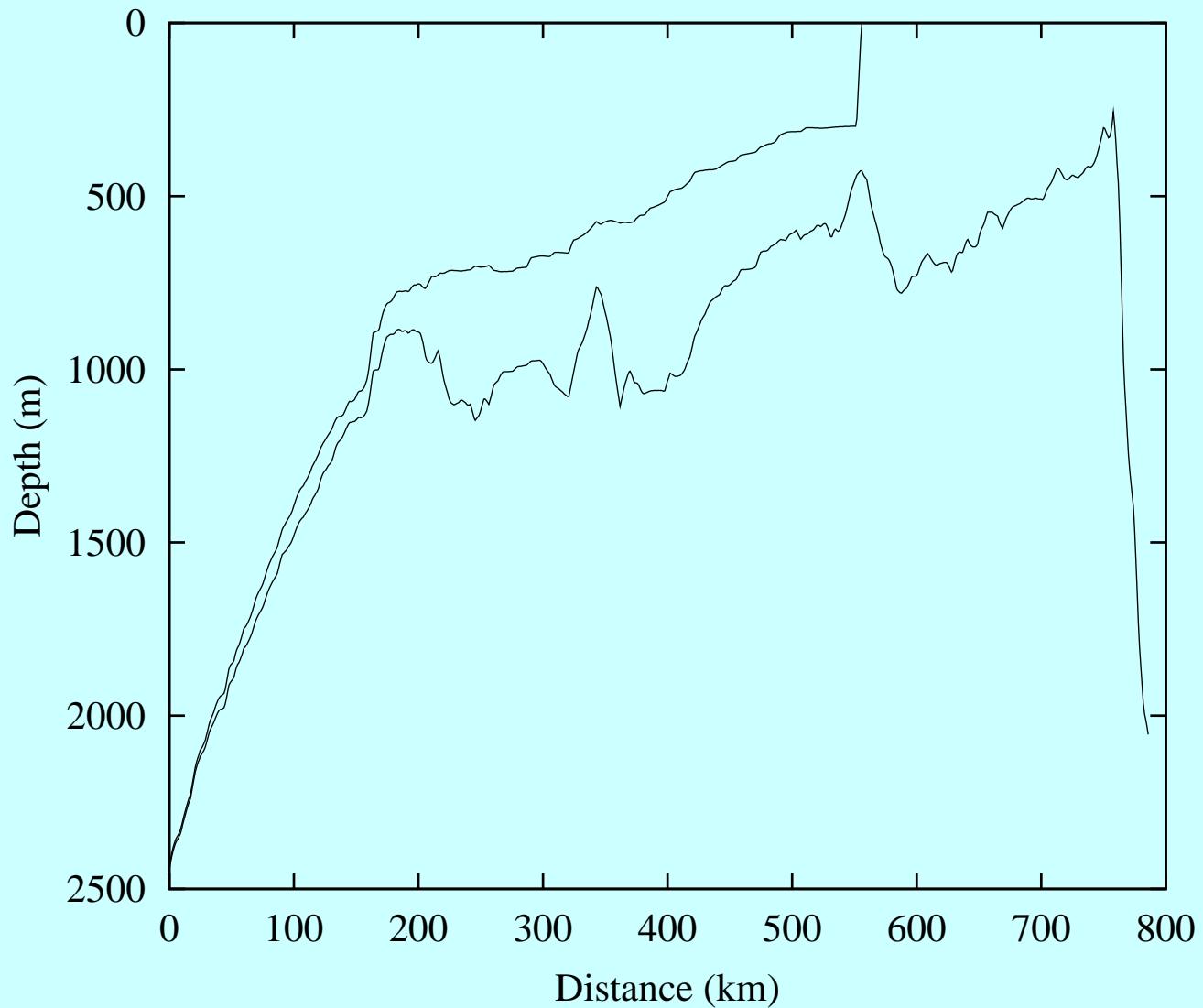
Bathymetry



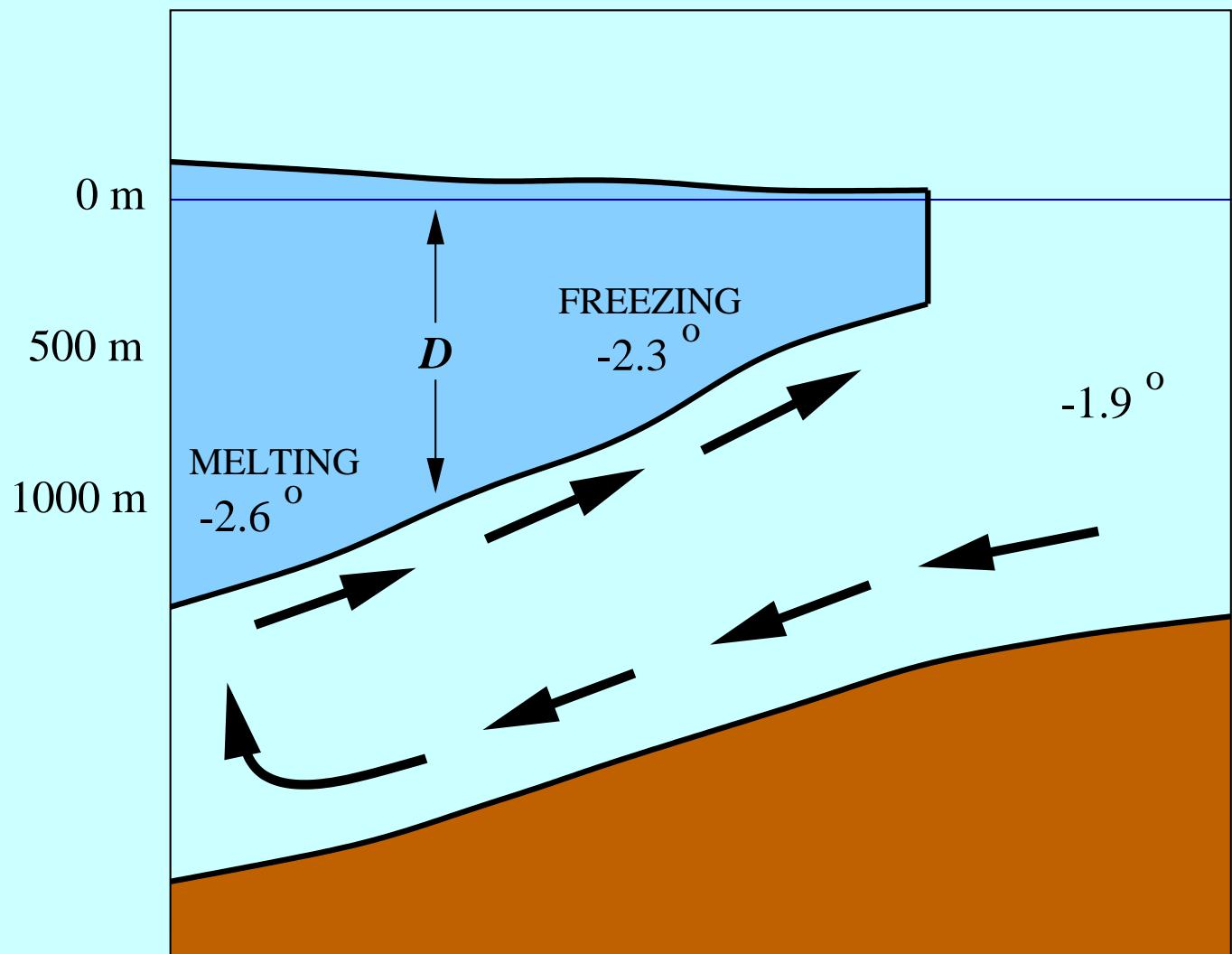
Water Column Thickness



Longitudinal Section



Melting and Freezing at the Ice/Ocean Interface



Why Are we Interested in the Cavity Under the Amery Ice Shelf?

- Part of a larger study of the mass balance of the Antarctic Ice Sheet, which includes modelling of the ice shelf itself.
- Rate of melting and refreezing under the ice shelf?
- Dependence of the above on global warming?

Model Requirements

- Currents: average \approx tidal $\approx 0.02 \text{ ms}^{-1}$
- Large range of depth
- Large range of ice draft
- Large range of water column thickness
- Boundary layers associated with both bottom and ice/ocean interface
- Area: 59,000 km²; Average water column thickness: 215 m
- Rossby radius: 5,000 m
- e-folding time of cavity ≈ 3 years. Hence model runs of about ≈ 14 years.

Hence require:

- Free-surface 3-D baroclinic model
- sigma- or isopycnic coordinates (to cope with topography and boundary layers)

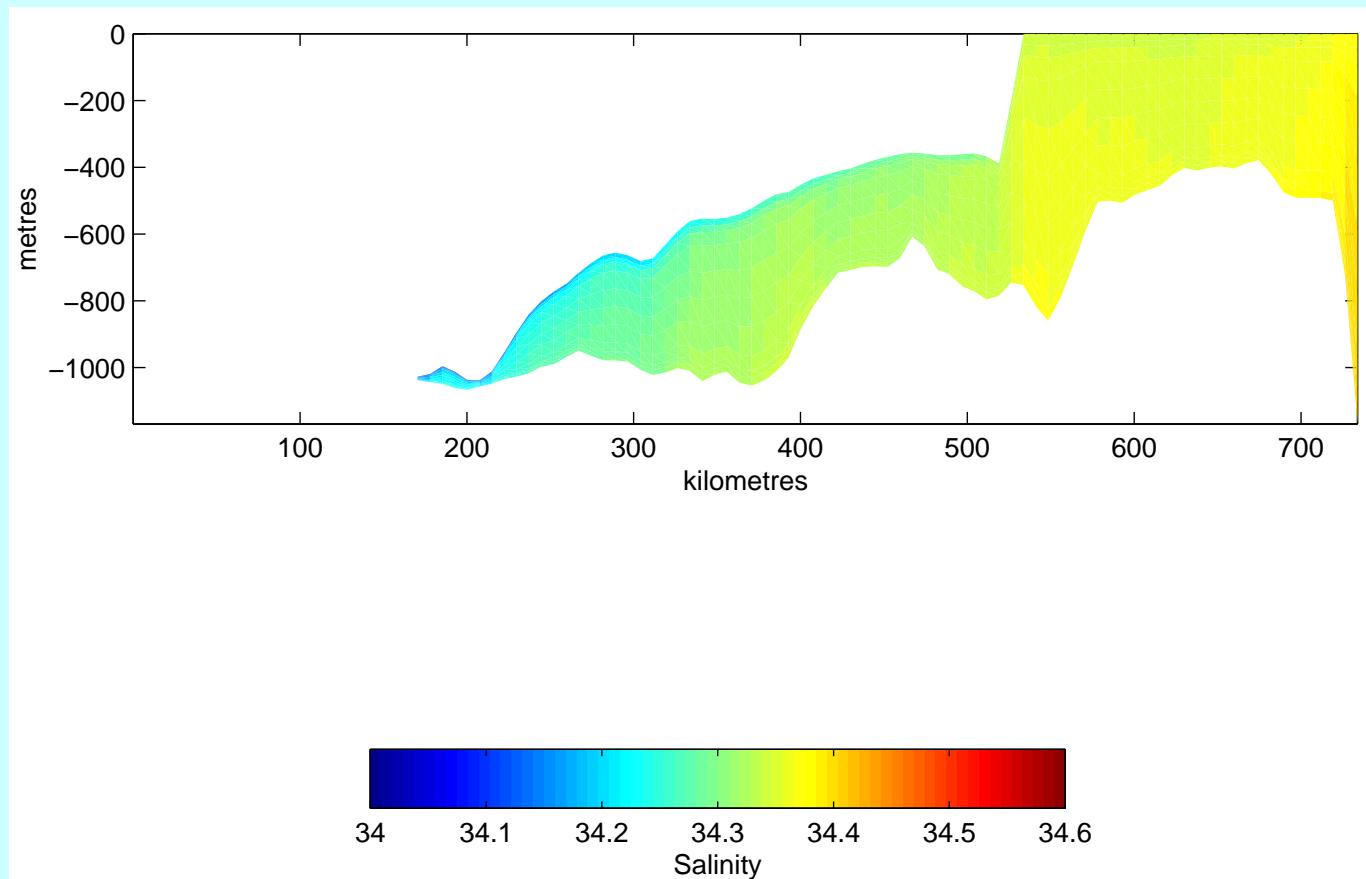
Solutions

- Grosfeld (Munster): Generalised coordinate version of Cox/Bryan (Gerdes) – Larsen and Filschner-Ronne, coupled with ice model
- Beckmann/Hellmer (AWI): SPEM/SCRUM/ROMS – whole Southern Ocean
- Holland (New York): MICOM (isopycnic) – Filchner-Ronne
- Present: POM – Amery.
Grid sizes: 4 km and 8 km.

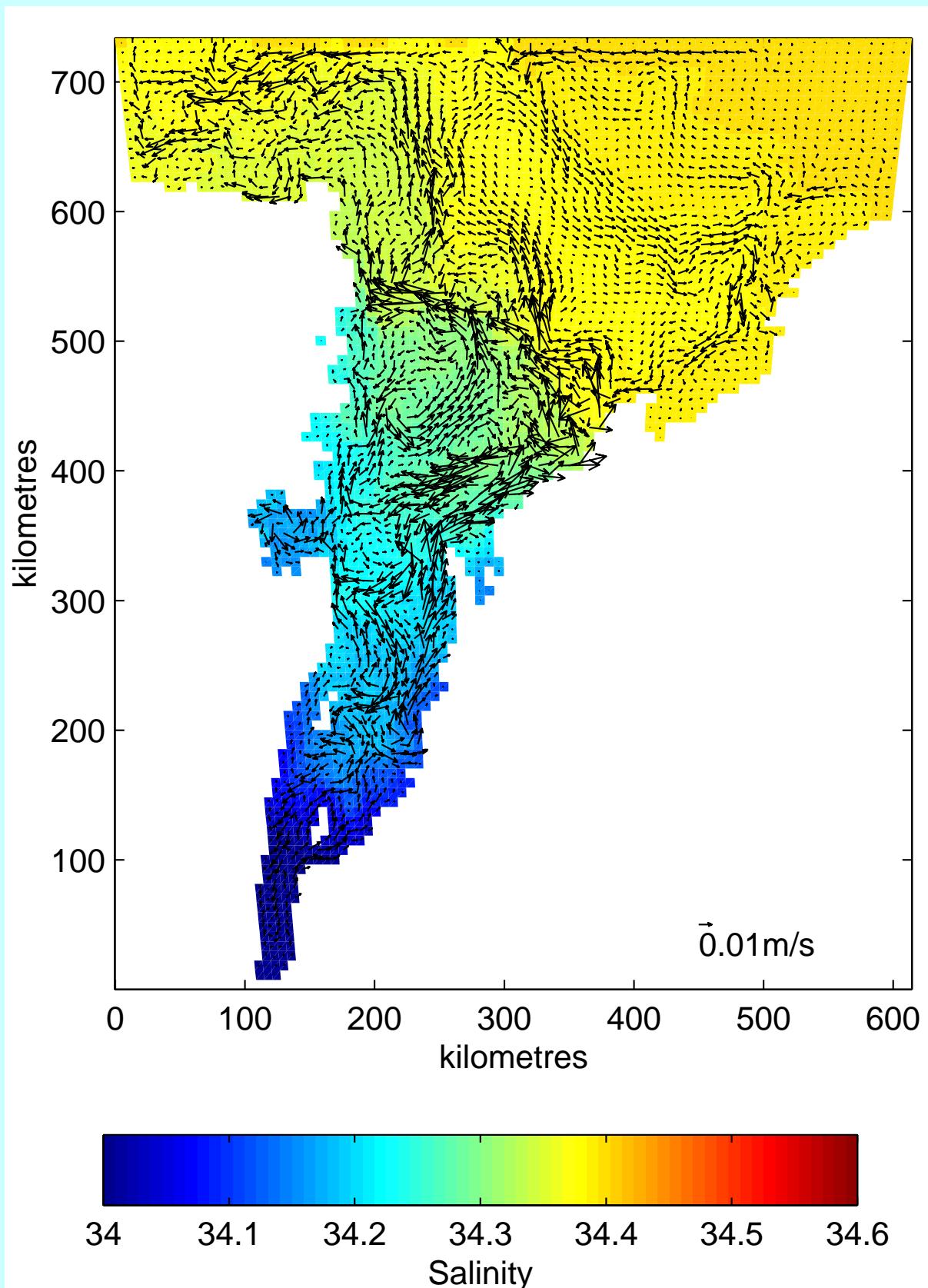
Required Modifications to Incorporate Ice Shelf into POM

- Define new ‘SEAMOUNT’ for initialisation.
- Define additional horizontal U, V and E masks for ice shelf.
- Apply surface pressure to depress ocean surface by D (i.e. apply adjustment D to all heights that are multiplied by g (GRAV), except in baroclinic pressure and buoyancy gradients).
- Dynamics at ice/ocean interface: invert bottom friction code (yields u_*).
- Thermodynamics at ice/ocean interface (2-equation formulation of Holland and Jenkins, 1999):
 - Interface assumed to be at local freezing temperature (T_f) (*converted to potential temperature*).
 - Heat flux assumed $\propto u_*(T_{ocean} - T_f)$.
 - Heat flux yields melting or freezing rate.
 - NOTE adjustments to resultant T and S fluxes to account for TBIAS and SBIAS.
 - Add source/sink of water to volume conservation equation in external mode.
 - Set $W(I,J,KB)=0$, reverse order of vertical integration of W and stop at $K=2$ (this puts source/sink of water in top cell).

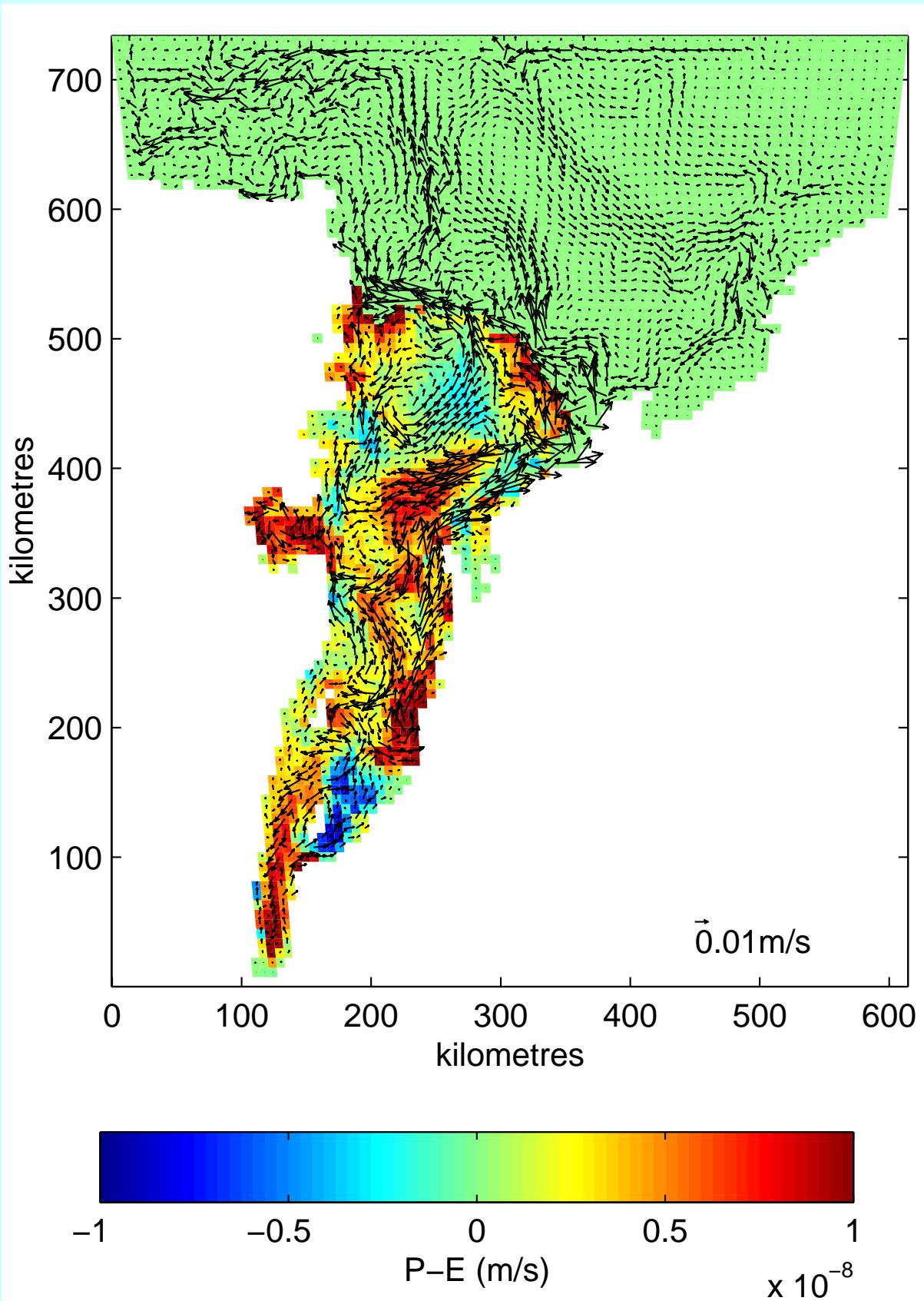
Initial Results – South-North Salinity Section



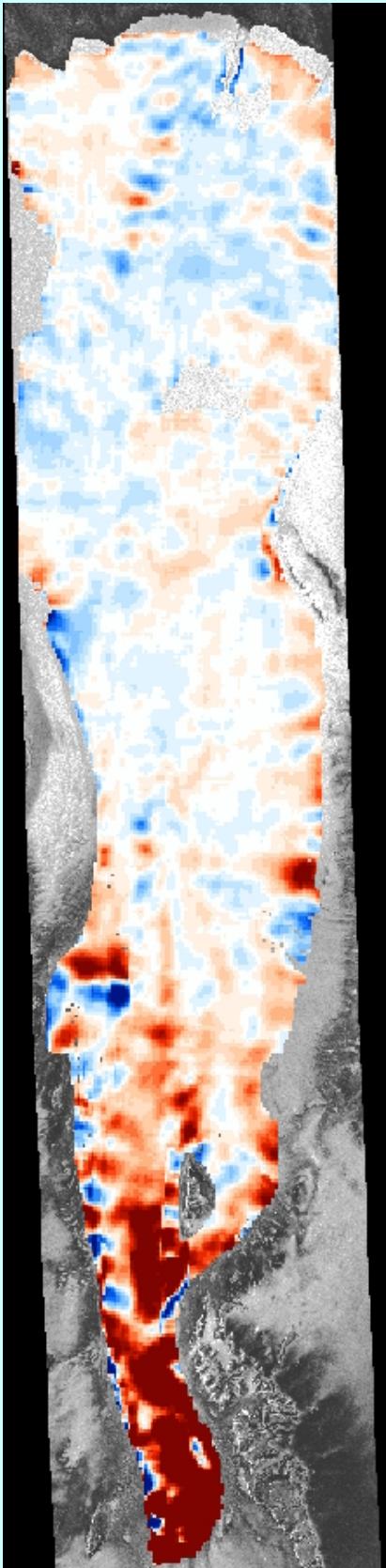
Initial Results – Salinity Map



Initial Results – Melting/Freezing (P-E) Map



'Observed' Melting/Freezing



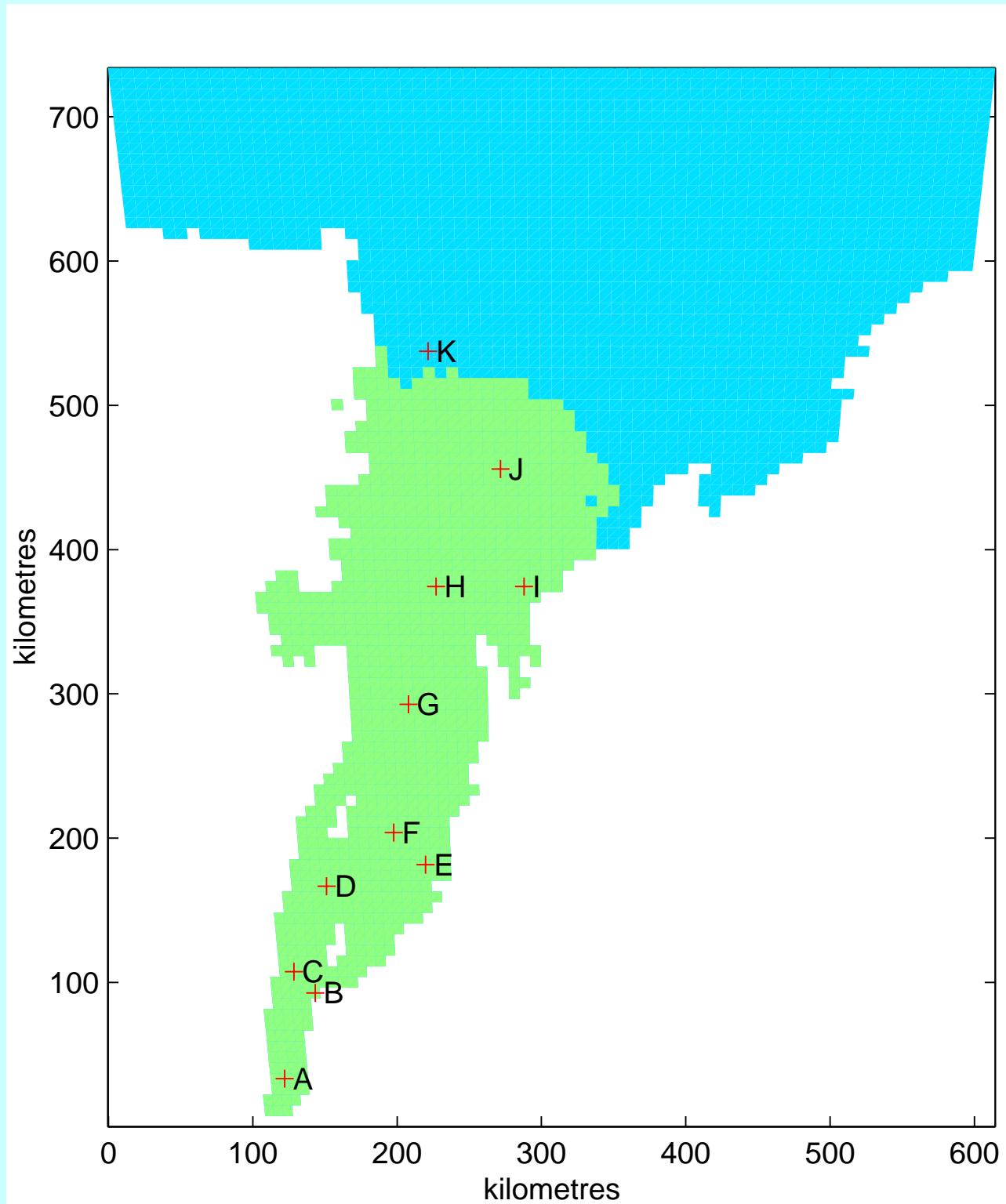
Red: 10 m/year
 $(3.2 \times 10^{-7} \text{ ms}^{-1})$
melting

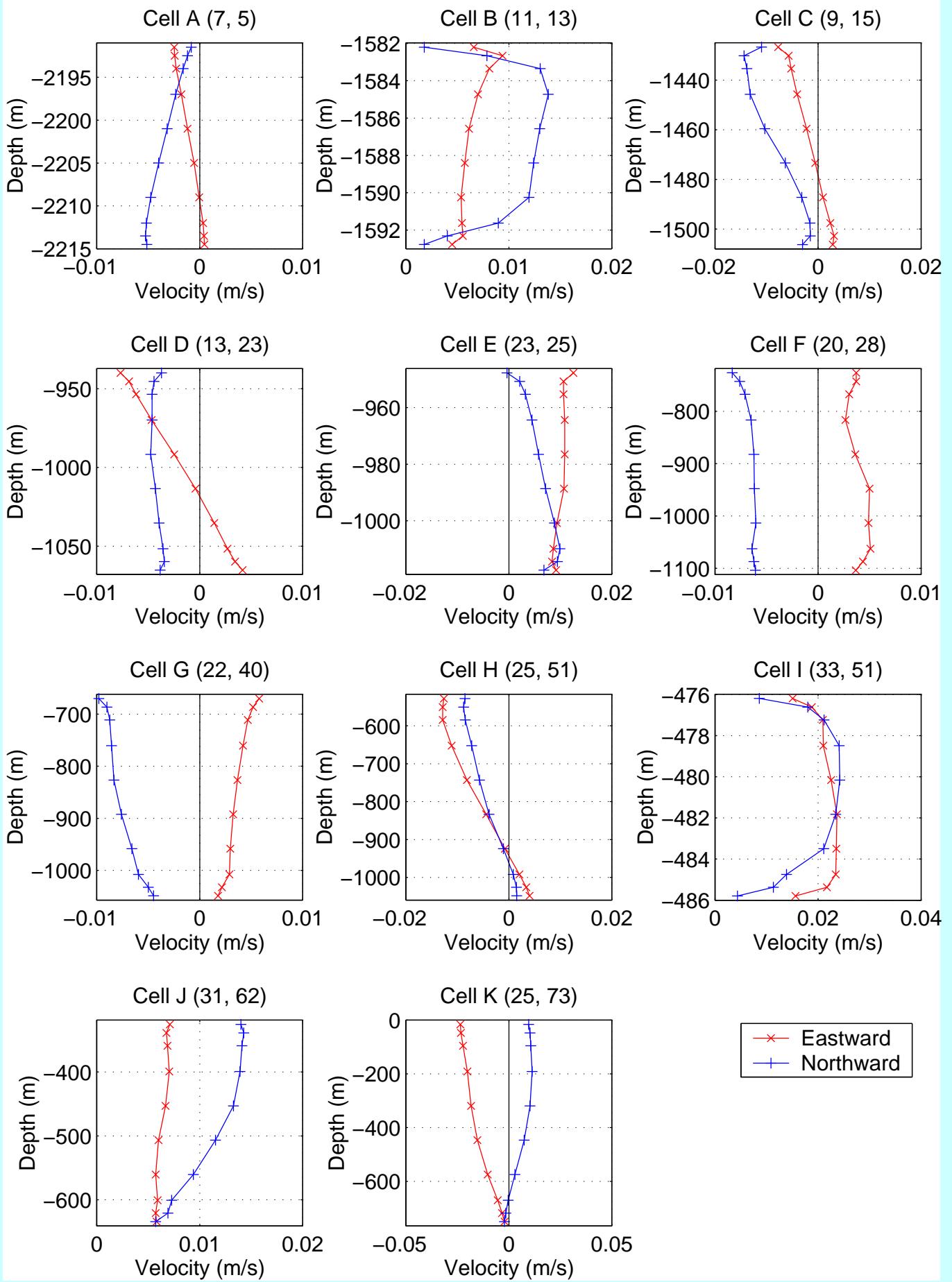
Blue: 10 m/year
 $(3.2 \times 10^{-7} \text{ ms}^{-1})$
freezing

Kinematic estimation
based on SAR,
altimetry and ice
density model

(Young, Hyland and
Gale)

Locations of Current Profiles

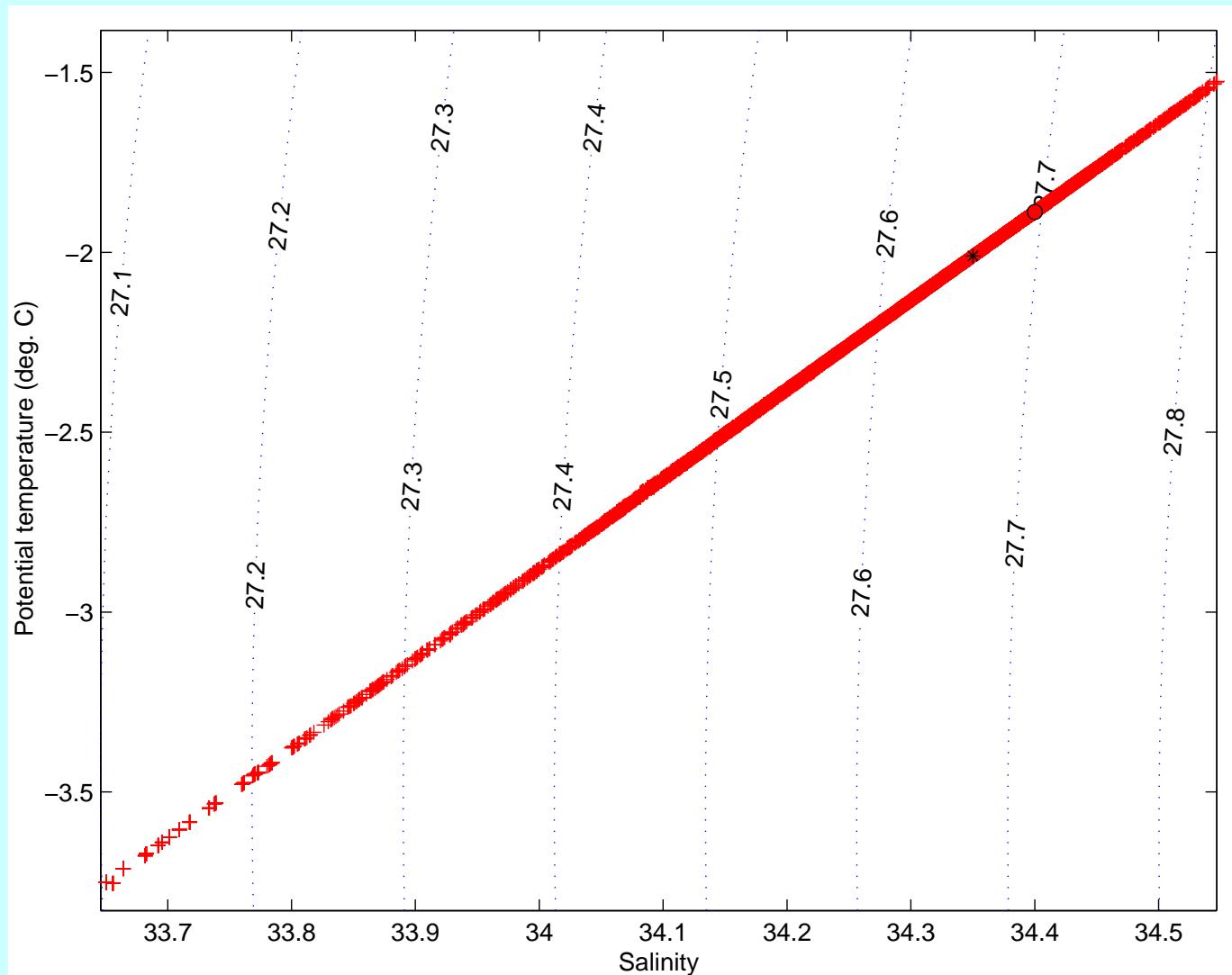




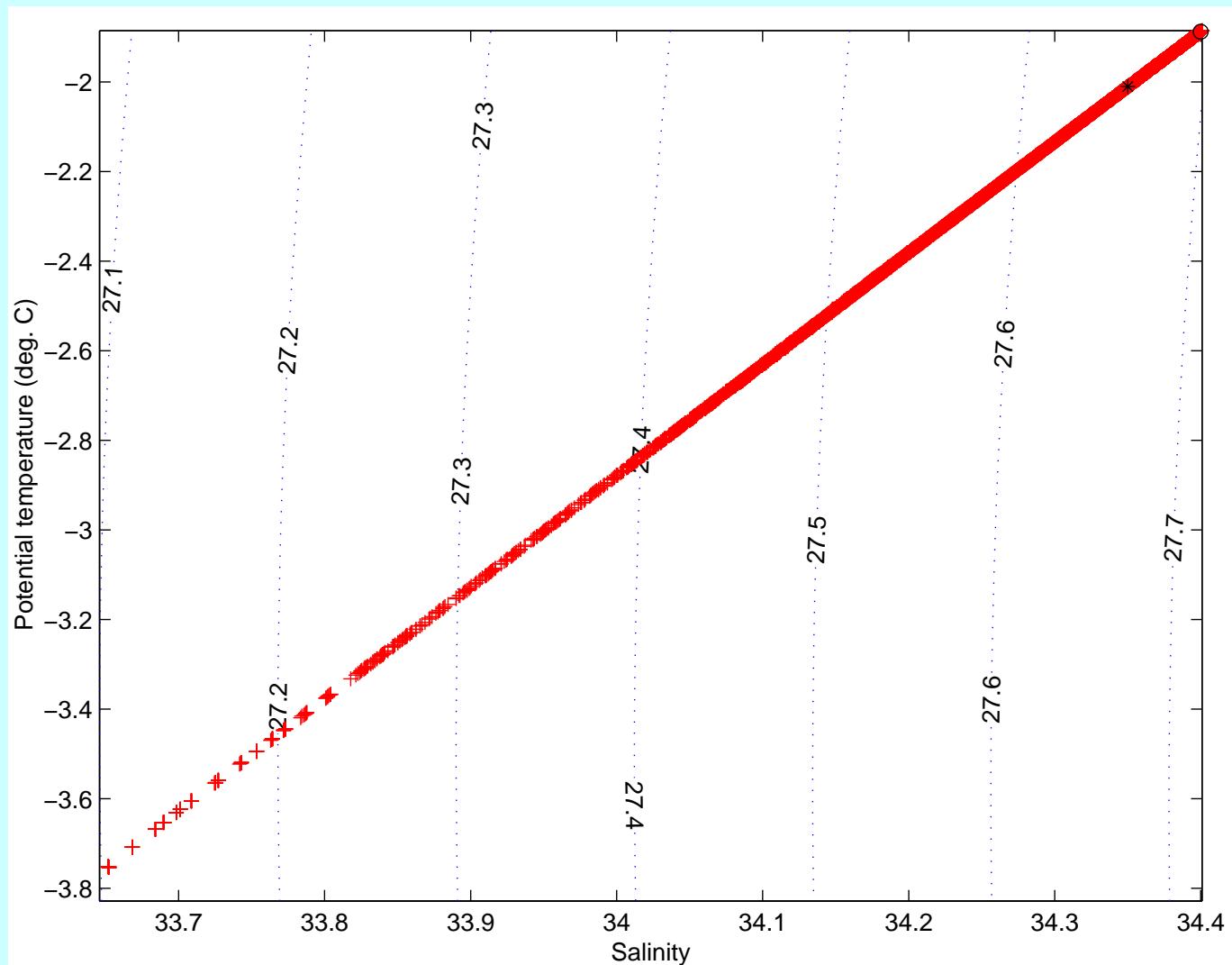
Advection Problem

- With initial conditions and ocean water at $T = -1.89^\circ$ and $S = 34.4$, there is *nothing warmer* within the model
- Hence water properties can only move in direction: $T < -1.89^\circ$ and $S < 34.4$
- ‘Ringing’ of centred advection scheme generates water with $T > -1.89^\circ$ and $S > 34.4$

T-S Diagram; Centred Differencing,
HORCON=0.5, Additional $(A_M, A_H)=100$



T-S Diagram; Smolarkiewicz,
HORCON=0.5, Additional $(A_M, A_H)=100$



Future Work

- Inclusion of tides (present melting/freezing rates are too low).
- Migration to ROMS?
- Model tuning and validation.
- Investigations of present and warming scenarios.
- Coupling with an ice shelf model.