

# If-less KPP

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**Jim McWilliams**

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- **Why KPP?**

- ...don't ask.

- **Why if-less?**

- if-switches may cause:

- discontinuities of second derivative

- discontinuities of first derivative

- discontinuities of function

- **hysteresis** and **multiple** solutions

- **To what extend if-less?**

- ...identify and eliminate the most offending ones

- ...this is a data-assimilation workshop.

## KPP boundary layer model:

Extent of PBL  $h_{bl}$  is determined from bulk Richardson number (LMD94)

$$Ri_b(z) = \frac{\Delta z g [\rho(z) - \rho_r] / \rho_0}{|\mathbf{u}_r - \mathbf{u}(z)|^2 + V_t^2(z)} \quad Ri_b(-h_{bl}) = Ri_{cr} = 0.3$$

after which  $h_{bl}$  is checked against Monin-Obukhov  $h_{MO} = u_*^3 / (\kappa \cdot B_f)$ , and Ekman  $h_{EK} = 0.7u_* / f$  depth and limited by both of them in the case of stable buoyancy forcing  $B_f > 0$ .

Once  $h_{bl}$  is known  $K_{m,s}(z) = w_{m,s} \cdot h_{bl} \cdot G(z/h_{bl})$  where  $G(\cdot)$  is universal non-dimensional shape function and  $w_{m,s} = \kappa u_* \cdot \psi_{m,s}(zB_f/u_*^3)$ .

- relies on Monin-Obukhov similarity theory
- KPP a bulk, non-local model of intermediate complexity
- a quasi-equilibrium, diagnostic model
- multi-process model
- widely used (CCM, POP, MIT, OPA); mostly for climate modeling

## Evolution of KPP: Summary of changes in KPP since 1994 by W. Large and G. Danabasoglu (2003), (2005):

- Turbulent velocity scale limit in **stable** regime
- Diurnal cycle in SW Rad. heat flux
- Critical bulk  $Ri$  depends on vertical resolution
- $C_v$  depends on BVF
- Correct Ekman and Monin-Obukhov depth limit computations
- Compute interior convection **after** BL mixing is done
- Modify usage of  $N$  in turbulent shear computation
- Quadratic interpolation of  $Ri$  to find  $h_{bl}$
- Monin-Obukhov depth limit is considered for elimination

## Motivation

### Early ROMS solution exhibit biases in thermocline depth

- too shallow in most cases

### Overall excessively sensitive to numerical discretization

- $h_{bl}$  fields are too noisy
- resolution drift:  $h_{bl}$  tends to go deeper with grid refinement

### Sources of discontinuous behavior:

- $Ri_b(z)$  oscillates if  $\mathbf{u}(z)$  is Ekman spiral (prevented only by  $h_{EK}$ -limit)
- hysteresis  $h_{MO}$  limitation logic
- hysteresis  $h_{EK}$  limitation logic
- vertical grid-point locking

### Integral formulation of PBL

- $Ri_b(z)$  disregards velocity profile and 3D-nality within PBL

### Calibration and tuning

- parameterization of elementary processes
- 1D experience
- 3D experience

**Criterion for finding  $h_{bl}$ :** We define surface PBL as an integral layer within which net production of turbulence due to shear-layer instability is balanced by dissipation due to stratification,

$$Cr(z) = \int_z^{\text{surface}} \mathcal{K}(z) \left\{ \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 - \frac{N^2}{\text{Ri}_{cr}} - C_{Ek} \cdot f^2 \right\} dz' + \frac{V_t^2(z)}{z}$$

and search for crossing point  $Cr(z) = 0$ .

$$N^2 = -\frac{g}{\rho_0} \cdot \left. \frac{\partial \rho}{\partial z} \right|_{ad} \quad \text{is B-V frequency (} ad \equiv \text{adiabatic);}$$

$f$  is Coriolis parameter;  $C_{Ek}$  is a nondimensional constant;

$V_t^2(z)$  is unresolved turbulent velocity shear (same as in LMD94);

Integration Kernel  $\mathcal{K}(z) = \frac{\zeta - z}{\epsilon h_{bl} + \zeta - z}$  is to ignore contribution from

near-surface sublayer  $\epsilon h_{bl}$  where M-O similarity law is not valid (plays the same role as to distinguish between  $\rho_{ref}$  vs.  $\rho_{surf}$  in  $Ri_b$  of LMD94).

$\zeta$  is free surface;  $\epsilon = 0.1$ .

- Same result as  $Ri_b$  the case of linear velocity profile, but otherwise

$$\int_{z'}^{z''} \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 dz \geq \frac{|\mathbf{u}'' - \mathbf{u}'|^2}{z'' - z'}$$

- $Cr(z)$  is **monotonic** for Ekman spiral  $\Rightarrow$  no sudden jumps of  $h_{bl}$
- Numerically more attractive, since  $\mathbf{u}(z)$  and  $\rho(z)$  can be reconstructed as continuous functions
- Avoids introduction of *reference* potential density: basically integration Brunt-Väisälä frequency. Allows formalism of *adiabatic* derivatives and differences to achieve monotonicity
- Correct account for thermobaric effect: Bill Large: to determine extent of BL one must bring water parcel **from reference depth to**  $z = -h_{bl}$  and compare its density with the ambient fluid **there**. We never did it this way in ROMS community (?)
- Avoids ambiguity for merging top and bottom BLs

## Pure physical limits:

destabilizing vs. stabilizing effects:

- balance  $\left| \frac{\partial \mathbf{u}}{\partial z} \right|^2$  vs.  $\frac{N^2}{\text{Ricr}}$   $\Rightarrow$  shear layer instability

- $\left| \frac{\partial \mathbf{u}}{\partial z} \right|^2$  vs.  $C_{\text{Ek}} \cdot f^2$   $\Rightarrow$  turbulent Ekman layer

- *negatively* forced  $\frac{N^2}{\text{Ricr}}$  vs.  $V_t^2$   $\Rightarrow$  free convection



**Monin-Obukhov depth limit**  $h_{bl} \leq h_{MO} = \frac{C^{MO} \cdot u_*^3}{\kappa \cdot B_f}$  if  $B_f(z) > 0$ .

Because of solar radiation absorption, buoyancy forcing  $B_f = B_f(z)$  increases with depth, possibly changing sign *from unstable to stable*  $\Rightarrow$  a case when  $B_f(-\text{overestimated } h_{bl}) > 0$ , but  $B_f(-h_{MO}) < 0 \Rightarrow$  **hysteresis** and oscillations in  $h_{bl}$

**solution # 1:** (2003) use  $B_f = B_f(-h_{MO})$  in computation of  $h_{MO}$ , i.e. implicit search for  $k$  enclosing  $z^*$ , such that

$$z_k \leq z^* \leq z_{k+1} \quad \text{and} \quad h_{MO}(z_k) \leq |z^*| \leq h_{MO}(z_{k+1})$$

then solve 
$$\frac{h_{MOk}(z_{k+1} - z^*) + h_{MOk+1}(z^* - z_k)}{z_{k+1} - z_k} + z^* = 0$$

resulting in 
$$h_{MO} = -z^* = \frac{\frac{C^{MO} u_*^3}{\kappa} (B_{f'k+1} z_{k+1} - B_{f'k} z_k)}{B_{f'k+1} B_{f'k} (z_{k+1} - z_k) + \frac{C^{MO} u_*^3}{\kappa} (B_{f'k} - B_{f'k+1})}$$

above  $B_{f'} = \max(B_f, 0)$ ; if  $k$  not found  $\Rightarrow$  no limit; **no singularity** if either  $B_f \rightarrow 0$ ; limit applied **outside**  $B_f > 0$  **logic**: it is already taken into account in computing  $h_{MO}$ ; **since**  $h_{bl}$  **is not involved**  $\Rightarrow$  **no possibility of hysteresis**

**solution # 2:** (2005) Eliminate M-O limit altogether.

**Ekman depth limitation:**  $h_{bl} \leq h_{EK} = 0.7u_*/f$  for *stable* boundary layer; should be  $h_{bl} = h_{EK}$  for *neutral* forcing and stratification

Length  $\mathcal{L} = u_*/f$  and velocity  $\mathcal{U} = u_*$  are natural scaling parameters for neutrally stratified problem

$$i \cdot f \mathbf{u} = \frac{\partial}{\partial z} \left( w_m |z| \frac{\partial \mathbf{u}}{\partial z} \right)$$

where  $\mathbf{u} = u + iv$ , and  $w_m \equiv \kappa u_*$ , and  $\kappa$  is von Karman constant.

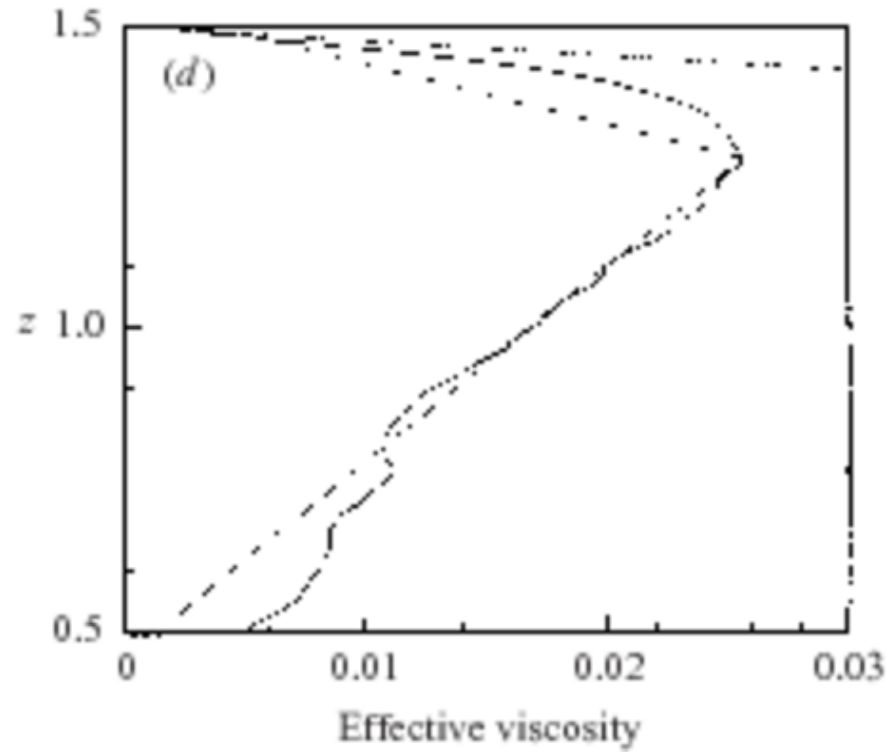
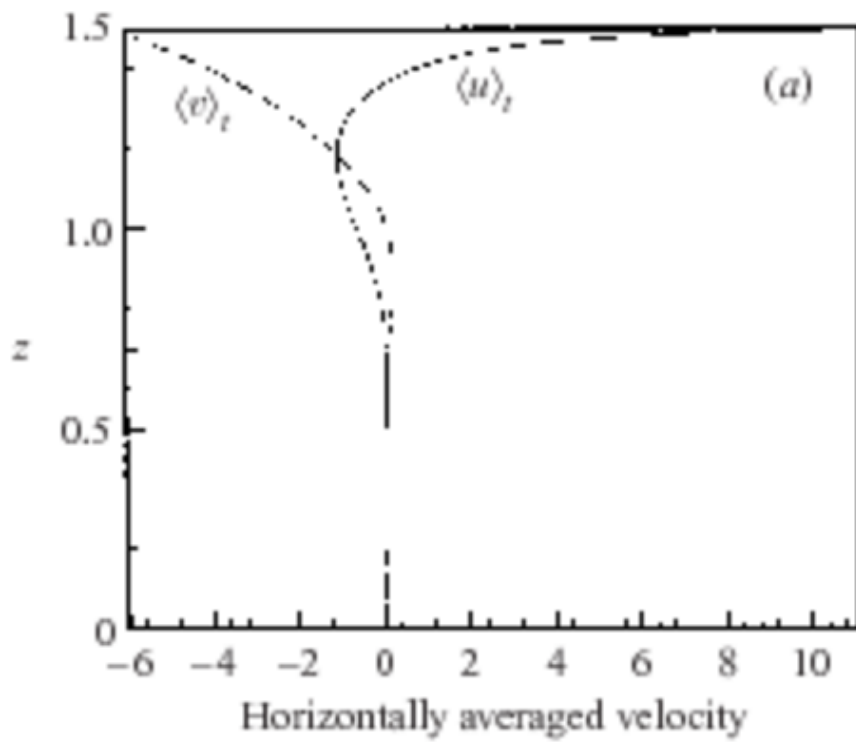
- Most vertical mixing schemes are "Coriolis-blind".
- Coriolis effect plays no role in determining  $h_{bl}$  via bulk Ri criterion;  $h_{EK}$ -limit is applied *a'posterio*ri, and only for stable buoyancy forcing.
- Because of light absorption, stability increases downward resulting in hysteresis if  $B_f(\text{unlimited } h_{bl}) > 0$ , but  $B_f(h_{EK}) < 0$  which is manifested by  $h_{bl}$  oscillations and jumps

??? integrate  $h_{EK}$ -limit into KPP BL criterion, balance

$$\int \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 dz' \quad \text{vs.} \quad \int f^2 dz' \quad ???$$

## DNS and LES simulations of Turbulent Ekman Layer:

- Zikanov, O., D. N. Slinn, and M. R. Dhanak, 2003: Large-eddy simulations of the wind-induced turbulent Ekman layer. *J. Fluid. Mech.*, **495**, 343-368.
- Esau, I., 2004: Simulation of Ekman Boundary Layers by Large Eddy Model with Dynamic Mixed Sub-filter Closure. *Envir. Fluid Mech.*, **4**, 273-303, DOI: 10.1023/B:EFMC.0000024236.38450.8d
- Coleman G. N., 1999: Similarity statistics from direct numerical simulation of the neutrally stratified PBL. *J. Atmos. Sci.*, **56**, 891-900.
- Coleman G. N., J. H. Ferziger, and P. R. Spalart, 1990: A numerical study of the turbulent Ekman layer. *J. Fluid. Mech.*, **213**, 313-348.
- Parmhed, O., I. Kos, and B. Grisogono, 2005: An improved Ekman layer approximation for smooth eddy diffusivity profiles. *Boundary-Layer Meteor.*, 115(3), 399-407.



DNS simulations from, Zikanov *et al* 2003.

**Modified Ekman problem:**  $i \cdot f \mathbf{u} = \frac{\partial}{\partial z} \left[ w_m \mathcal{L} G \left( \frac{z}{\mathcal{L}} \right) \frac{\partial \mathbf{u}}{\partial z} \right]$

$G$  is KPP non-dimensional shape function

$$G(\sigma) = |\sigma| (1 - \sigma)^2 + \begin{cases} \frac{(\sigma - \sigma_0)^2}{2\sigma_0}, & \sigma < \sigma_0 \\ 0 & \text{otherwise} \end{cases} \quad \sigma_0 = 0.1$$

B.C.:  $w_m \mathcal{L} G \left( \frac{z}{\mathcal{L}} \right) \frac{\partial \mathbf{u}}{\partial z} \Big|_{z=0} = u_*^2 \mathbf{1}_\tau \quad \Rightarrow \quad \frac{\partial \mathbf{u}}{\partial z} \Big|_{z=0} = \frac{u_* \mathbf{1}_\tau}{\kappa \mathcal{L} \sigma_0 / 2}$

$\mathbf{u} = 0$ , if  $z < -\mathcal{L}$

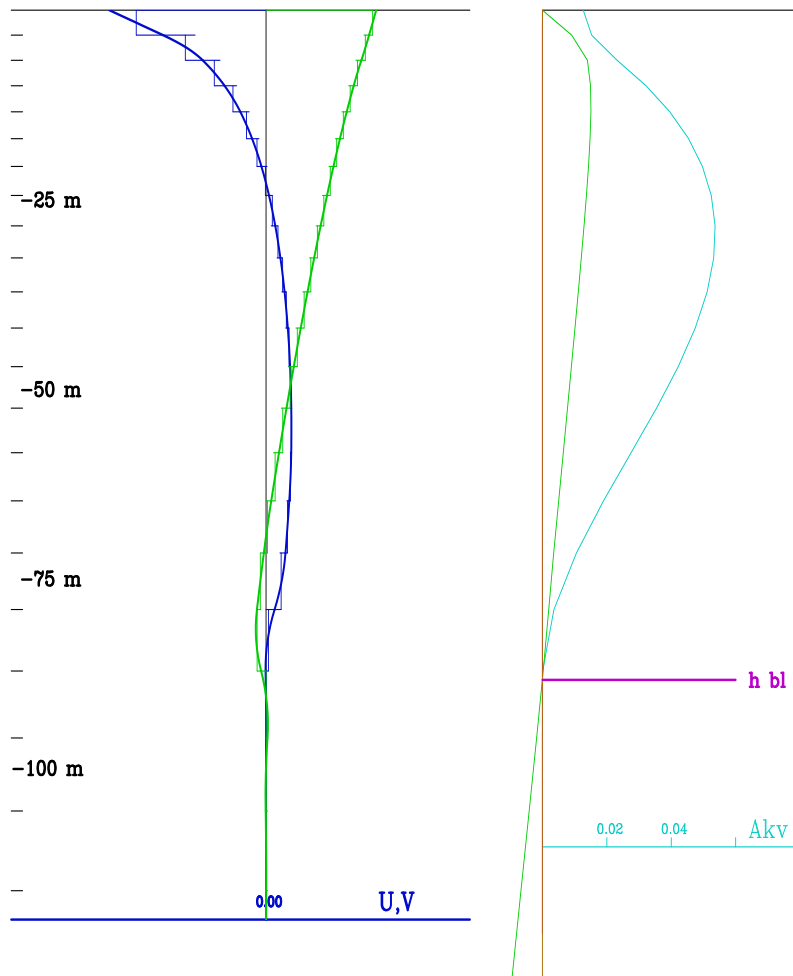
**Nondimensionalization:** Postulate that depth of generated this way boundary layer is equal to Ekman length and introduce scaling,

$$z = \mathcal{L} \sigma = \sigma \cdot 0.7 u_* / f \quad \mathbf{u} = u_* \cdot \tilde{\mathbf{u}},$$

hence

$$\frac{\partial}{\partial \sigma} \left( G(\sigma) \frac{\partial \tilde{\mathbf{u}}}{\partial \sigma} \right) = i \cdot \frac{\kappa}{0.7} \tilde{\mathbf{u}}, \quad \frac{\partial \tilde{\mathbf{u}}}{\partial \sigma} \Big|_{\sigma=0} = \frac{2}{\kappa \sigma_0}, \quad \tilde{\mathbf{u}} \Big|_{\sigma < -1} = 0$$

everything has been scaled out.



Recognize Coriolis force as *stabilizing* effect (balancing vertical shear production), construct

$$Cr(z) = \int_z^{\text{surf}} \mathcal{K}(z') \left\{ \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 - C_{EK} \cdot f^2 \right\} dz'$$

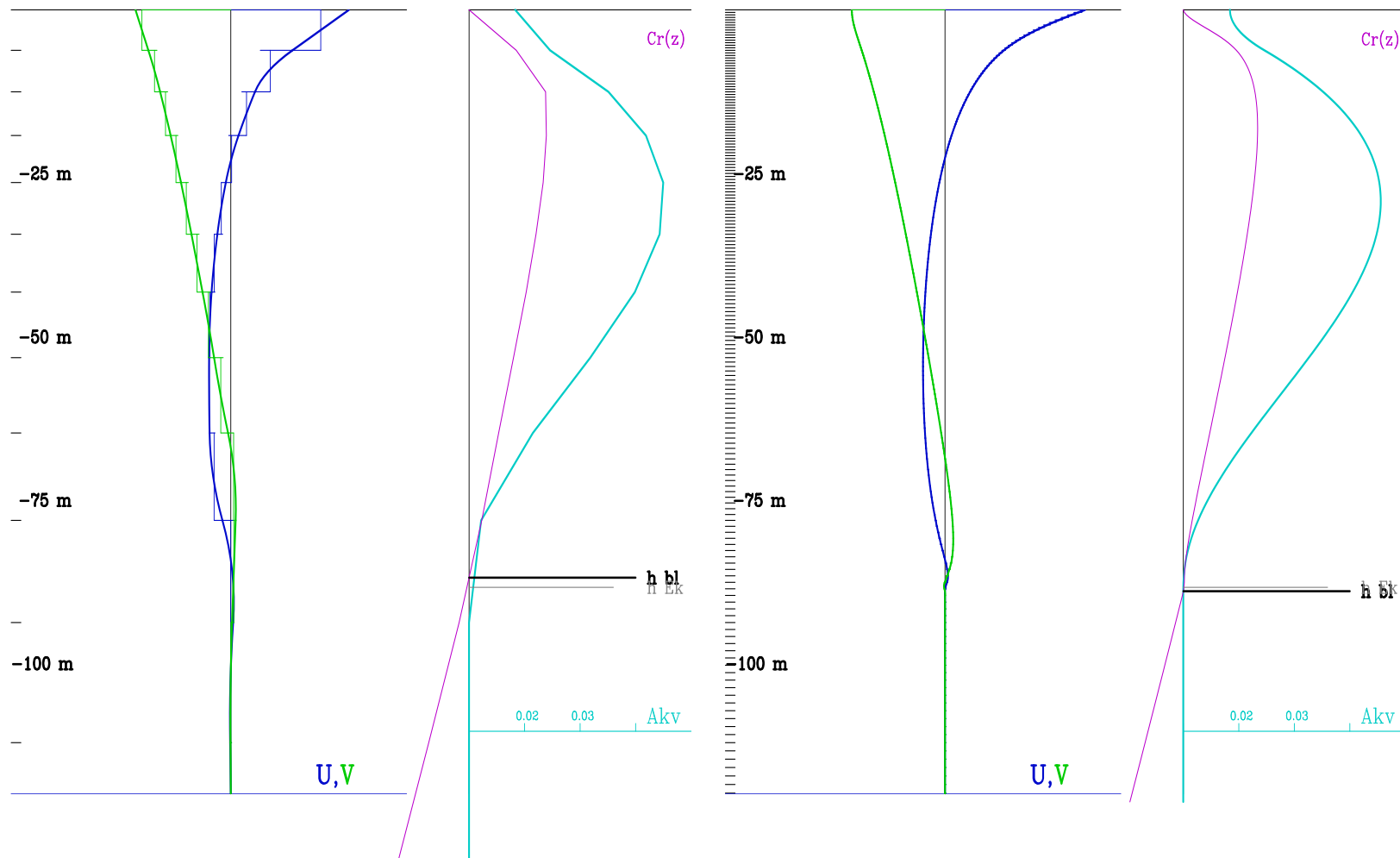
apply the same scaling

$$\widetilde{Cr}(\sigma) = \frac{1}{(0.7)^2} \int_{\sigma}^0 \mathcal{K}(\sigma) \left\{ \left| \frac{\partial \tilde{\mathbf{u}}}{\partial \sigma} \right|^2 - C_{EK} \right\} d\sigma'$$

and demand that  $\widetilde{Cr}(-1) = 0$ .

$C_{EK} = 258$  provided that

$\mathcal{K}(\sigma) = |\sigma| / (|\sigma| + \epsilon)$ , where  $\epsilon = 0.1$



Coarse,  $N = 32$  and fine,  $N = 512$  resolution.  $h_{EK}$  is shown for reference only and does not participate in determining  $h_{bl}$ .

- presence of  $\mathcal{K}(\sigma)$  is essential for convergence
- overall extremely robust

## Numerical Issues

velocities are smooth across  $z = -h_{bl}$ , **but tracers are not**

**Computation of  $Ri_b/Cr$  at vertical  $\rho$  vs.  $W$ -points:**

- $\rho$ -placement is natural for finite-difference (trapezoidal-rule) terms in  $Ri_b/Cr$  (but not for  $V_t^2$ ), however

$$A_{k+1/2} \sim \left( z_{k+1/2} - |h_{bl}| \right)^2$$

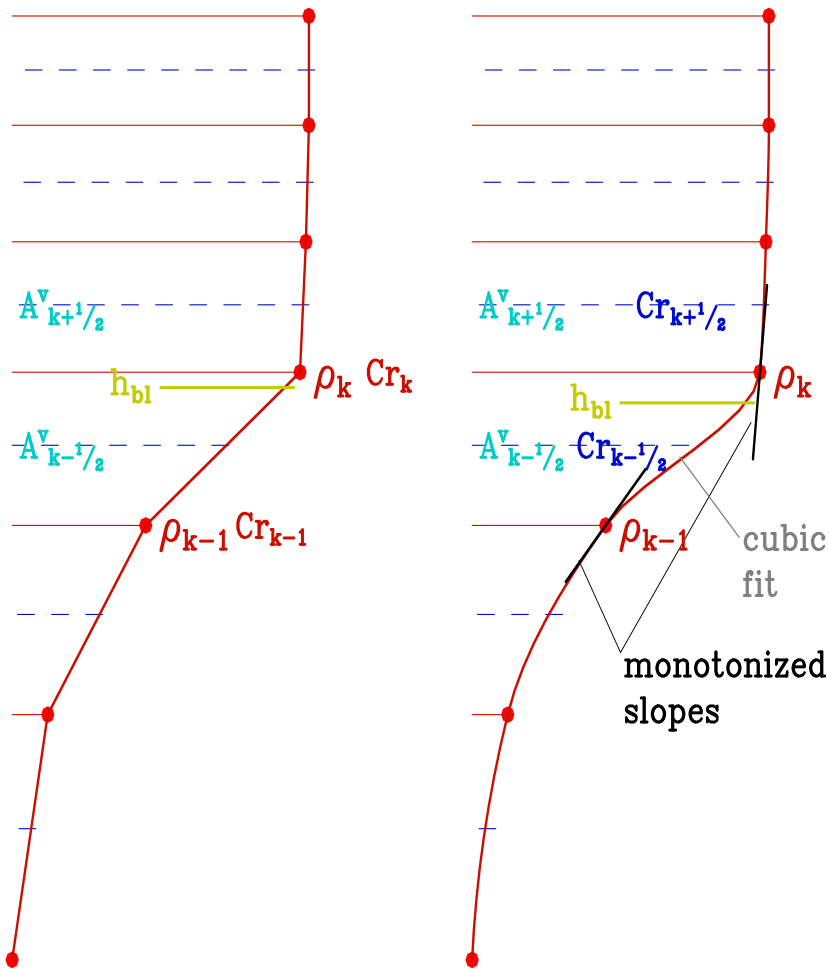
near the edge of PBL, hence needs  $h_{bl}$  needs accuracy relatively to  $W$ -points, while missing  $\rho$ -s is more forgiving

- Estimate  $V_t^2$  and  $Cr(z)$  at midpoints  $z_{k+1/2}$  using monotonized fit for bouyancy (integrated  $N^2$ ) to estimate its values and derivates at  $z_{k+1/2}$ -interfaces.
- *harmonic* averaging of *adiabatic* differences of density field (the same idea as for computing horizontal pressure gradient)

⇒ unlocking vertical steppiness

⇒ larger variation of PBL, typically shallower in summer





Monotonized reconstruction to compute  $V_t^2$  and  $\rho_{k+1/2}$ , but **not** to interpolate  $Cr$  to find  $h_{bl}$ : because of

$$Cr \sim w_s \sqrt{N^2 - N^2 d}$$

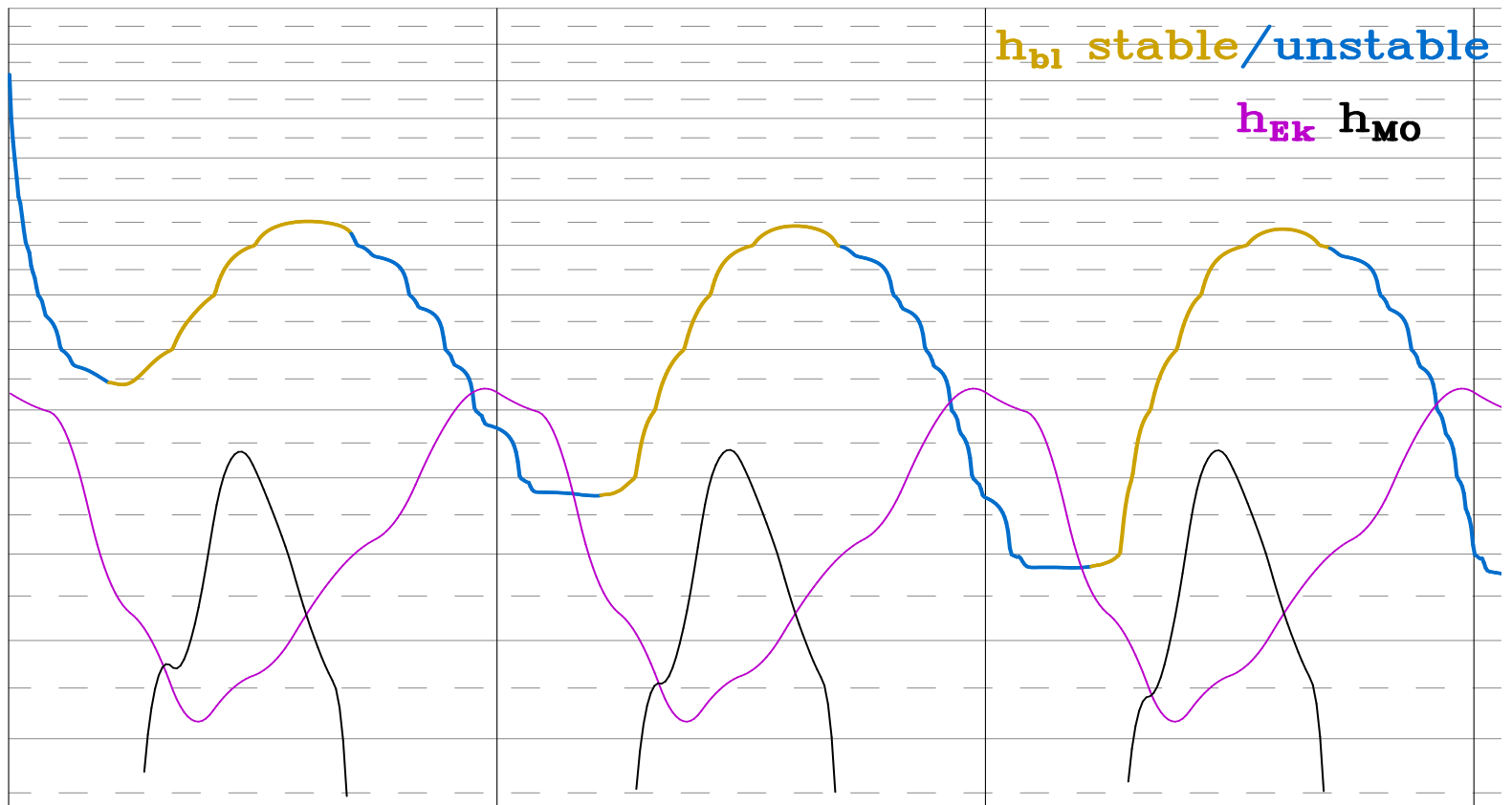
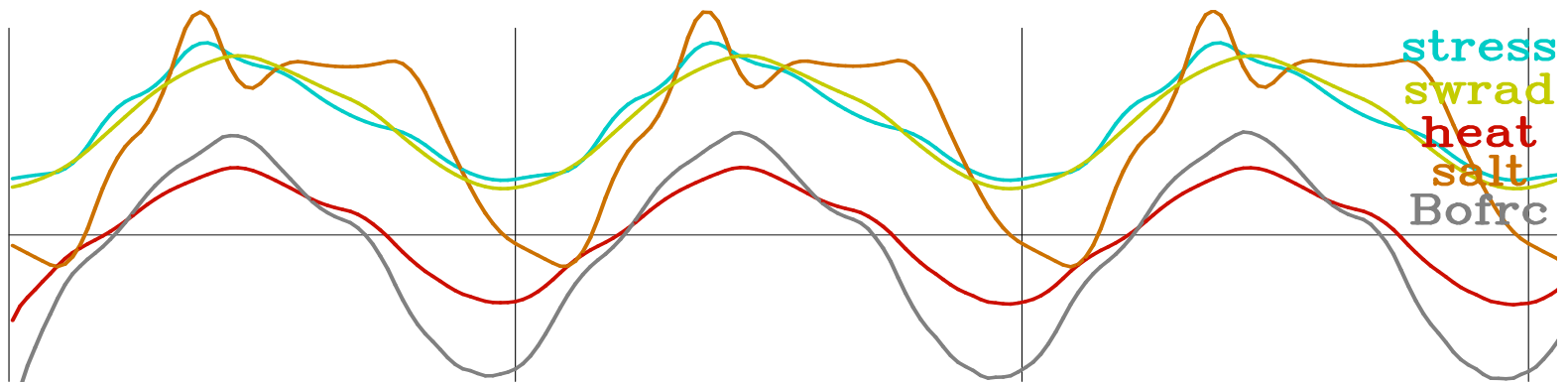
$Cr(z)$  is **not monotonic** near

$$z = -h_{bl}$$

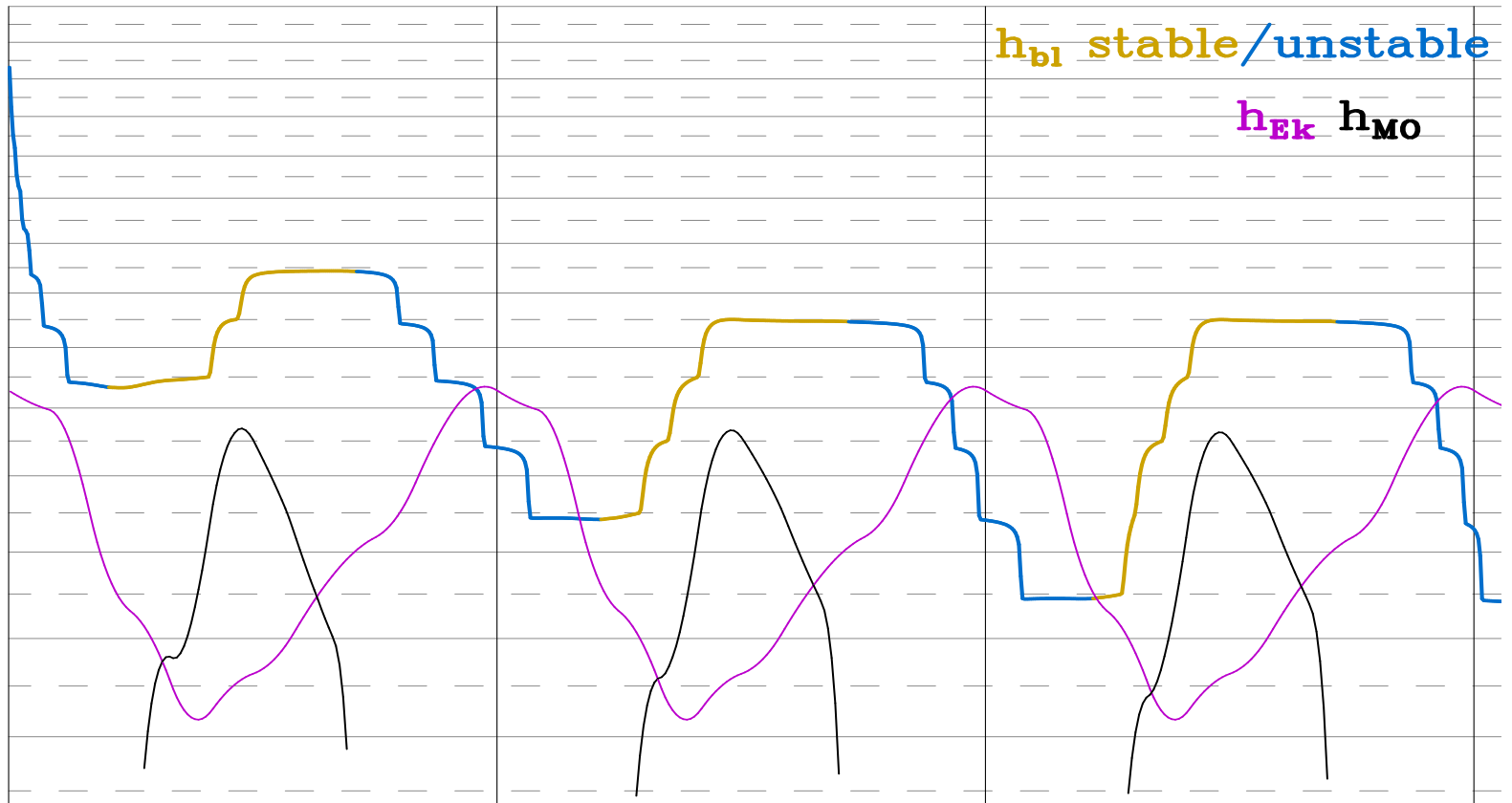
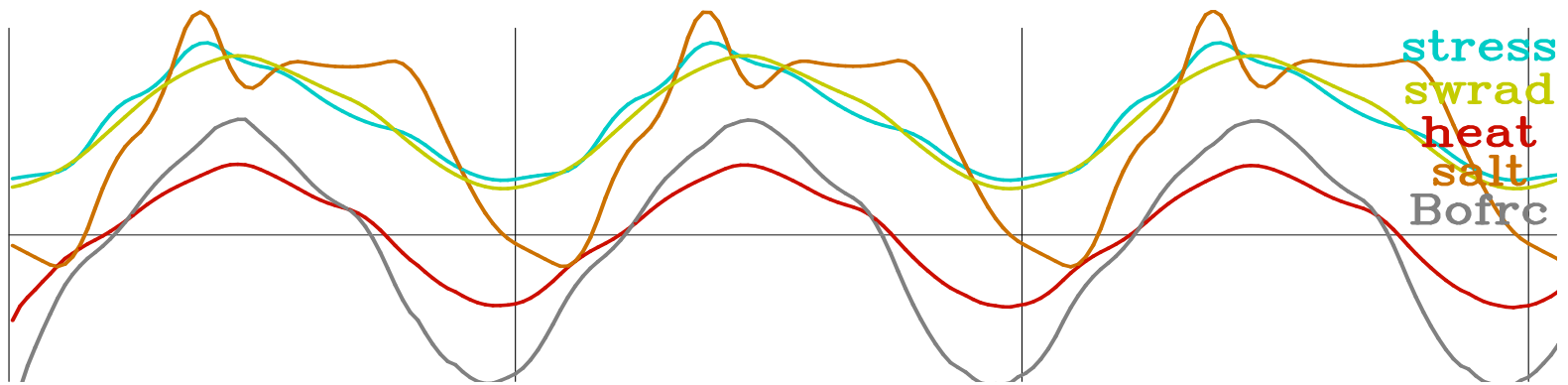
even if  $\rho(z)$  and  $u, v(z)$  are

$\Rightarrow$  quadratic (cubic) interpolation for  $Cr$  is dangerous

**Overall this is by far the largest cause of numerical sensitivities in KPP.**



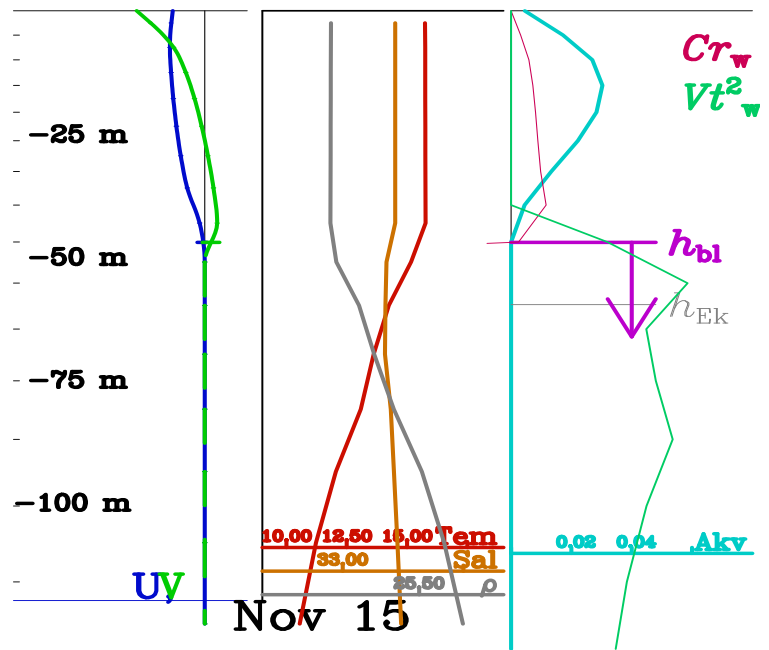
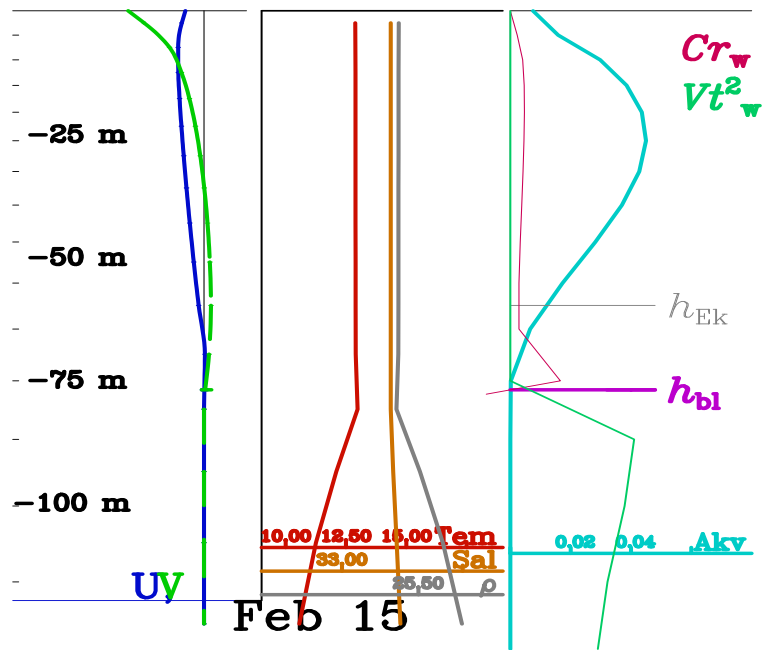
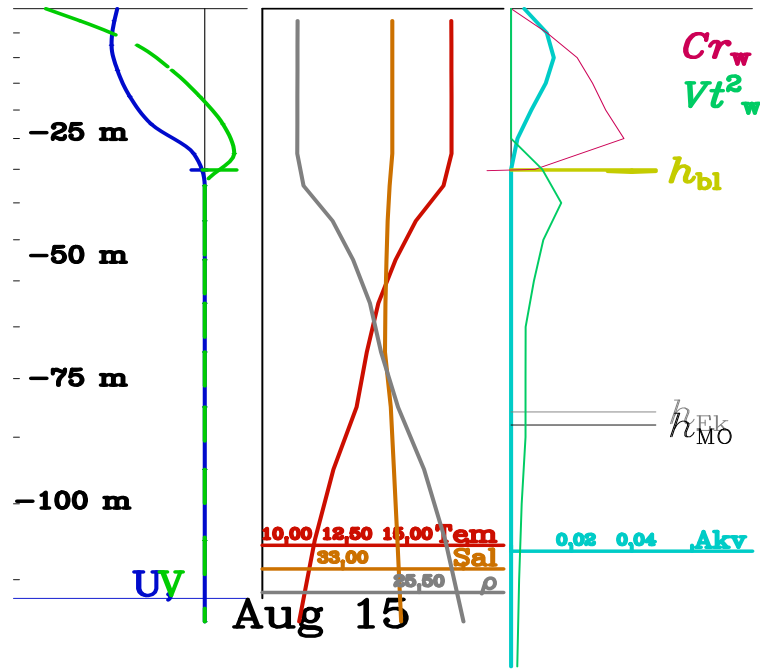
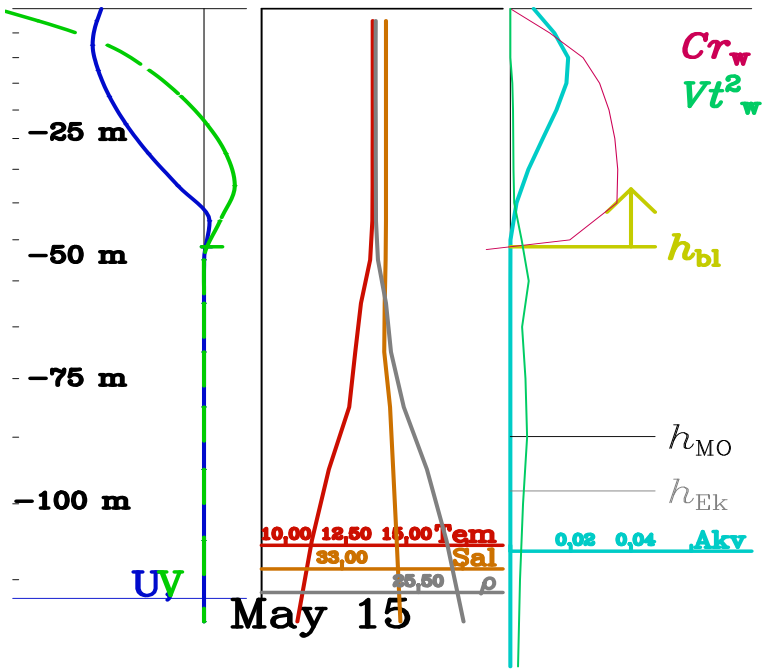
$Cr(z)$  at  $W$ -points,  $N = 40$

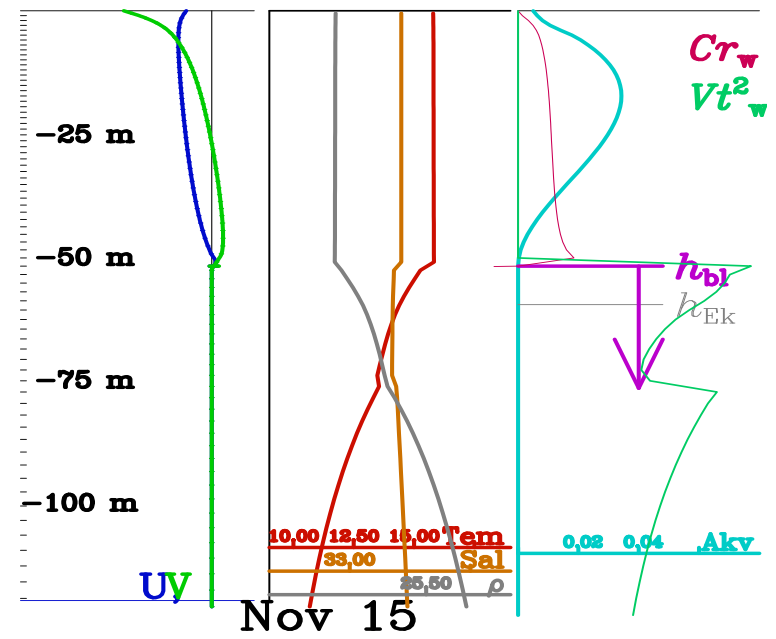
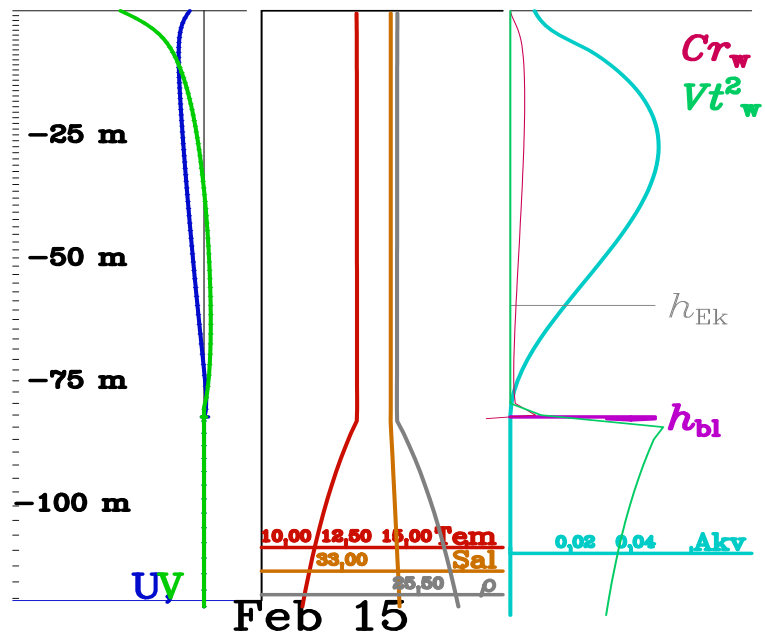
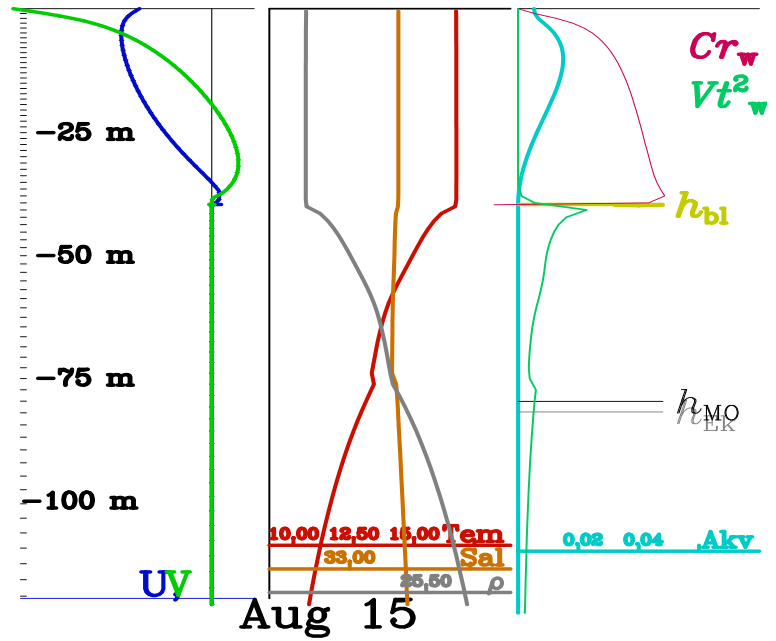
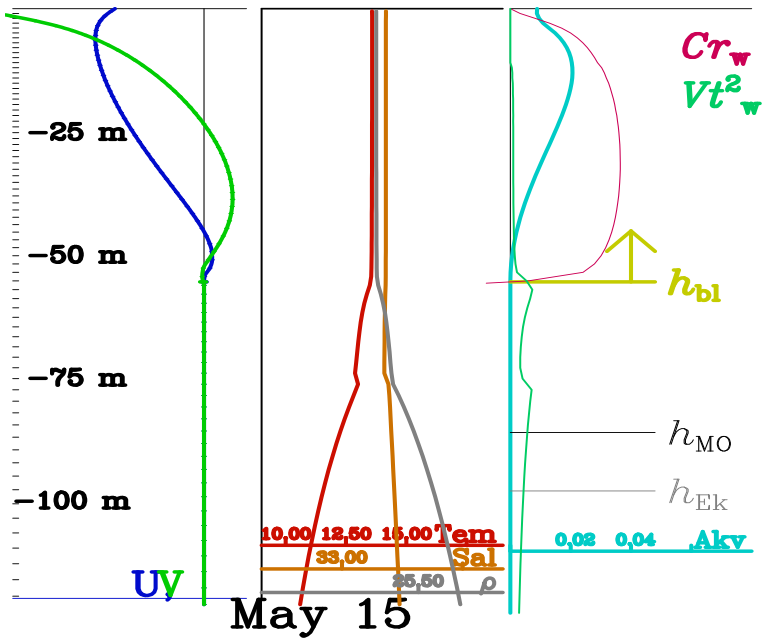


$Cr(z)$  at  $\rho$ -points,  $N = 40 \Rightarrow$  grid locking

# What it all adds up to?

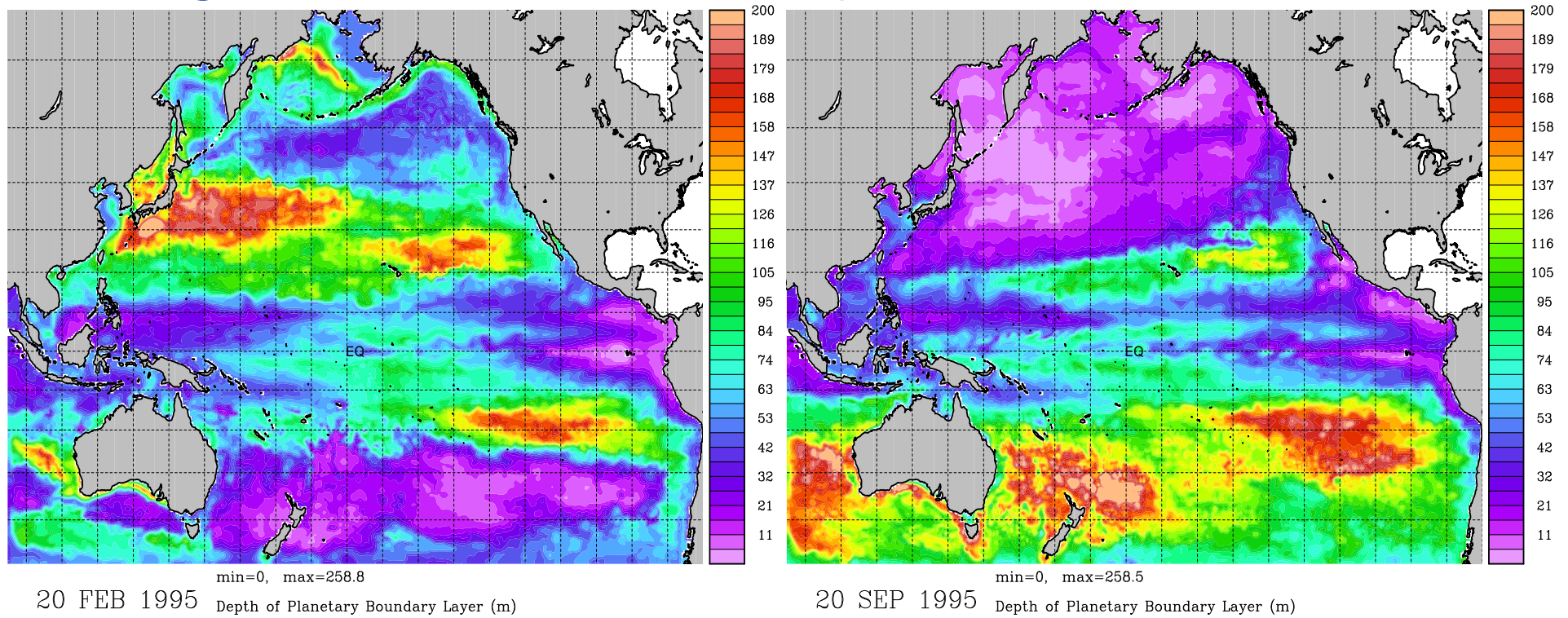
- 1D
- 3D
- comparison with reality





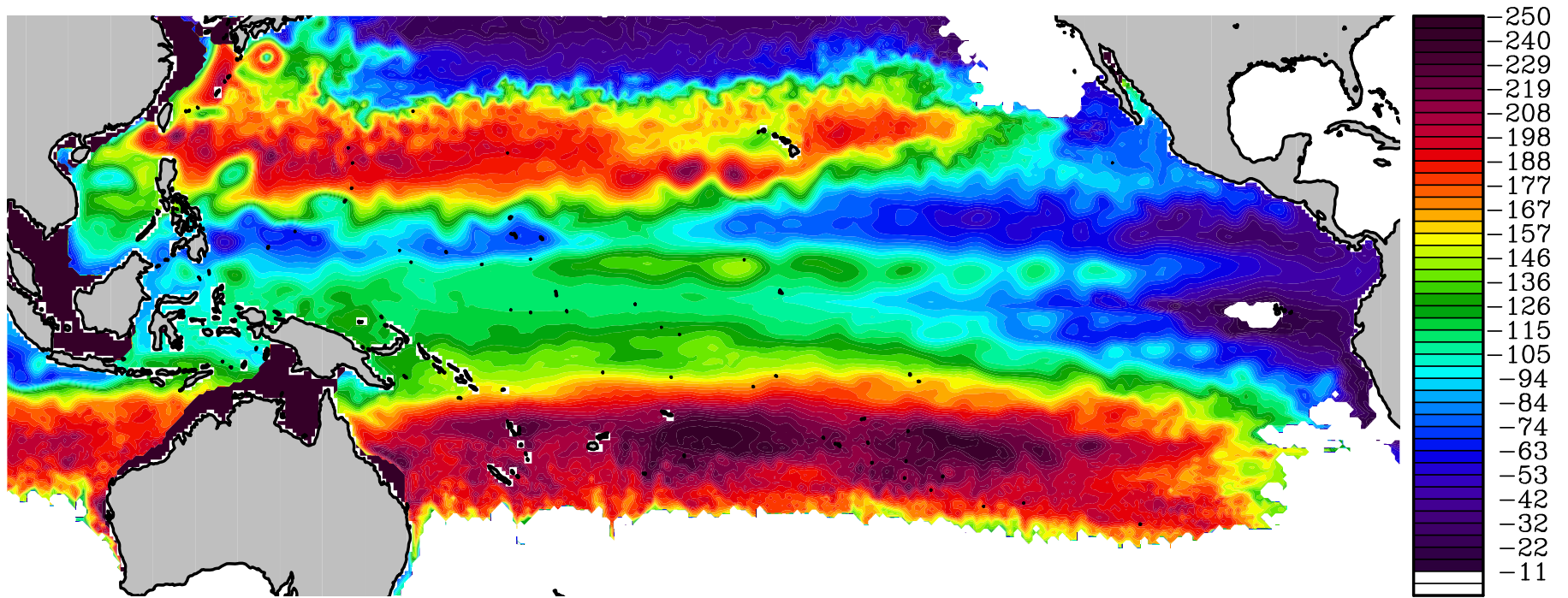
# 3D Modeling

## 0.45-degree Pacific Model forced by NCEP winds

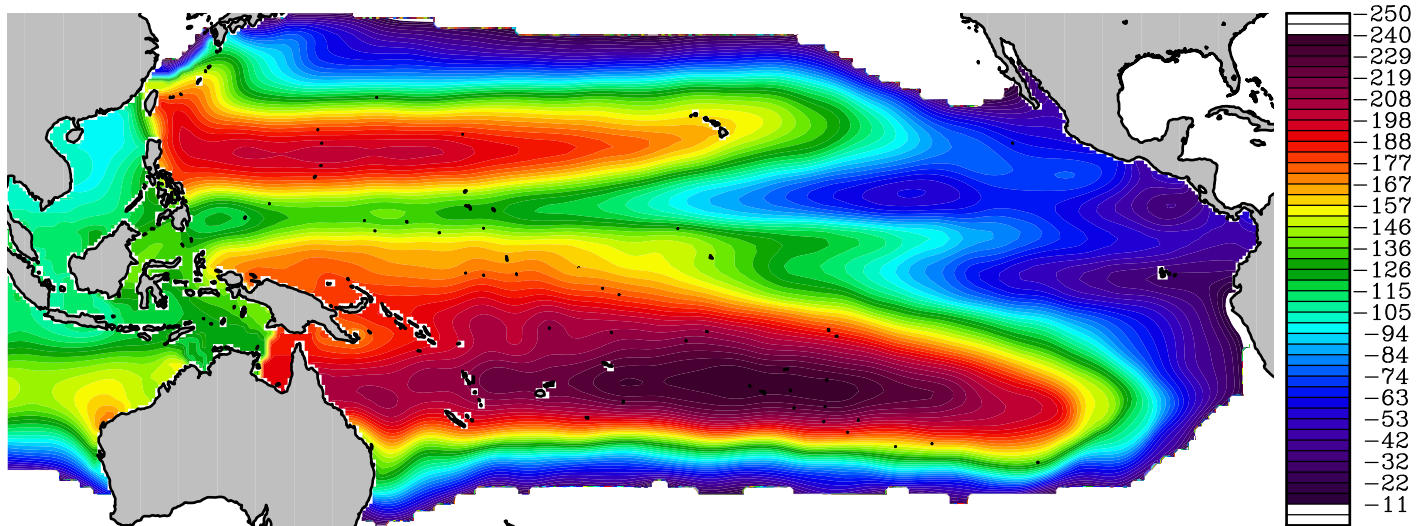


seasonal variation of  $h_{bl}$ -field



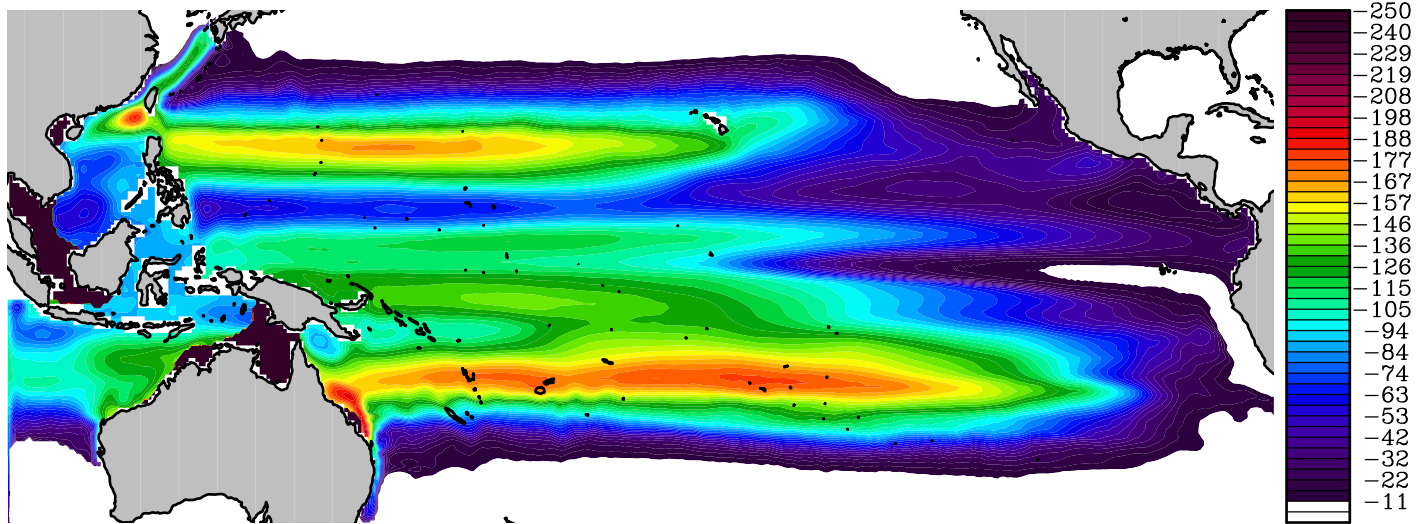


Depth of 20°C isotherm, instantaneous snapshot from a recent 2005 simulation



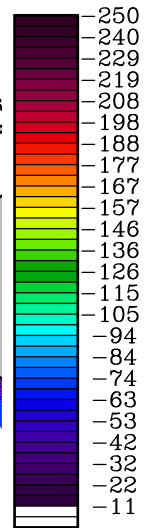
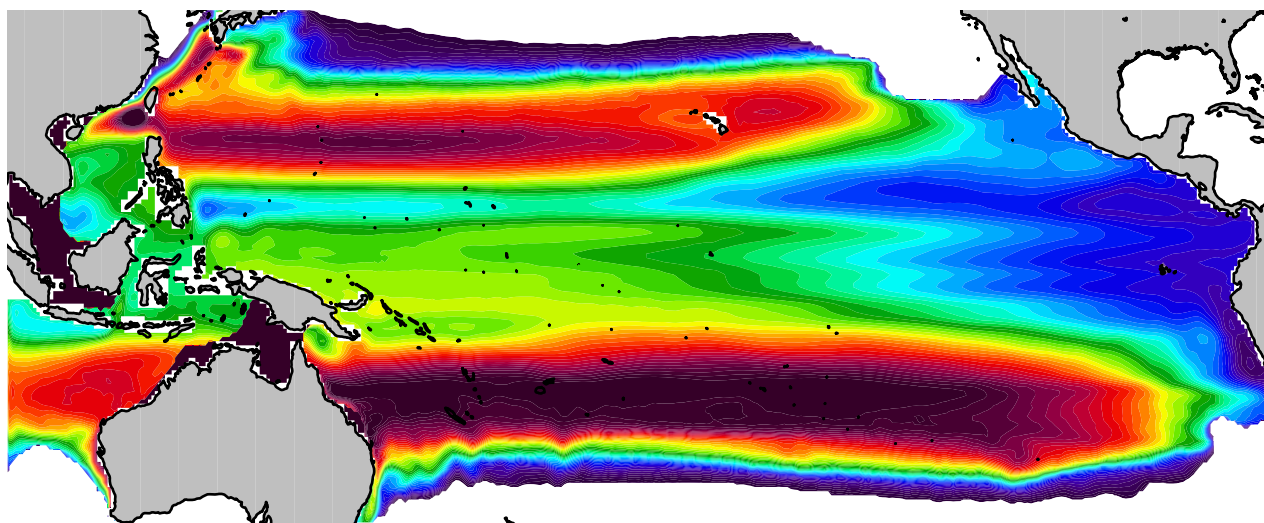
Depth of  
20°C isotherm,  
10-year  
annual mean

Levitus



vs.

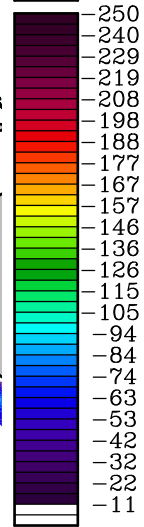
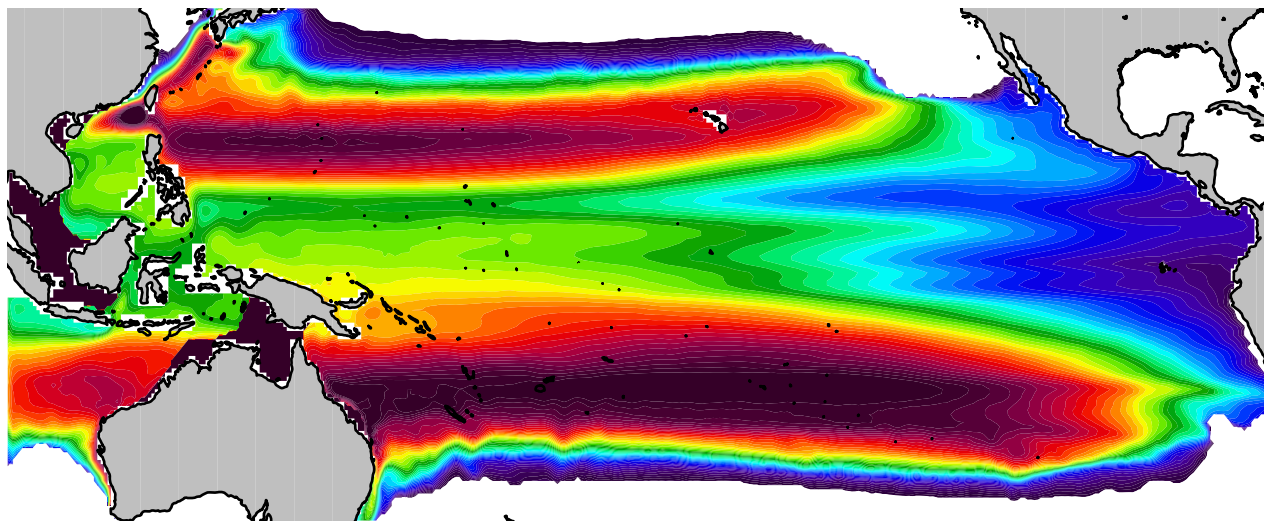
ROMS  
with early  
2003  
*baseline*  
KPP



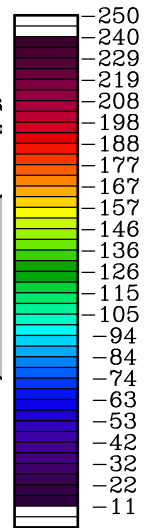
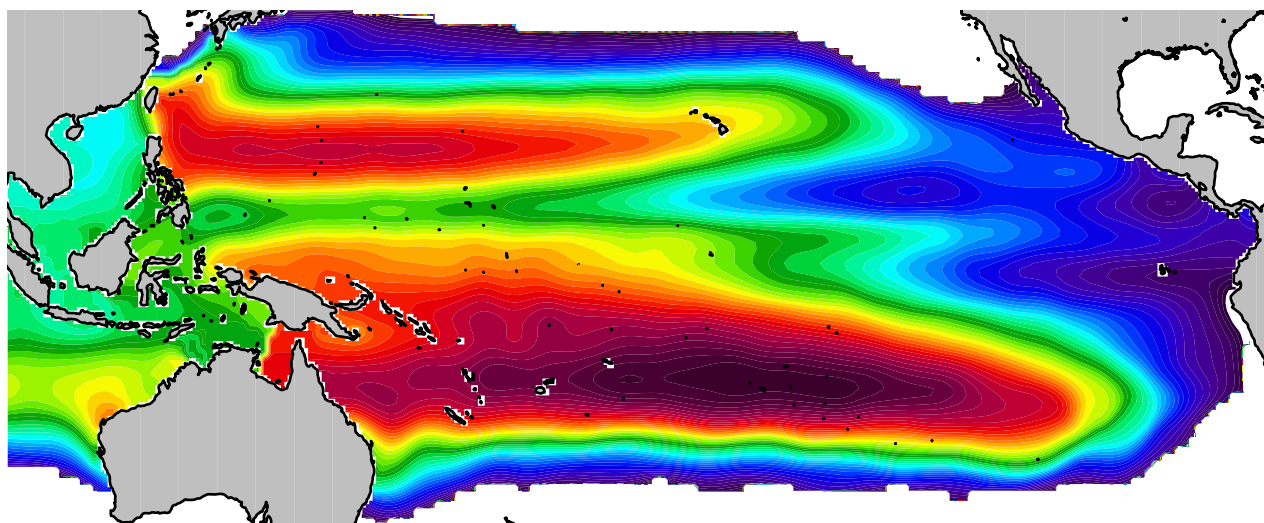
NCEP

vs.

ERS  
winds

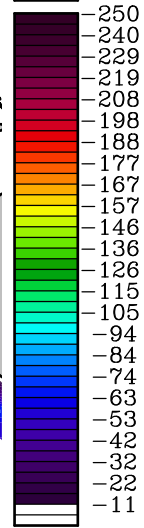
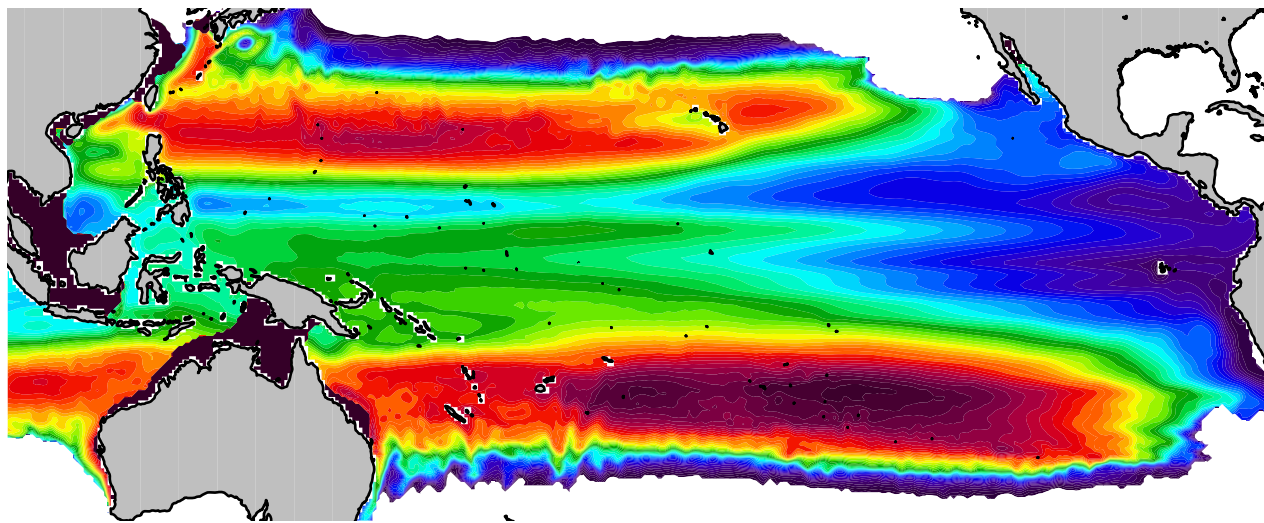


New KPP  
in both,  
 $Ri_{cr} = 0.45$

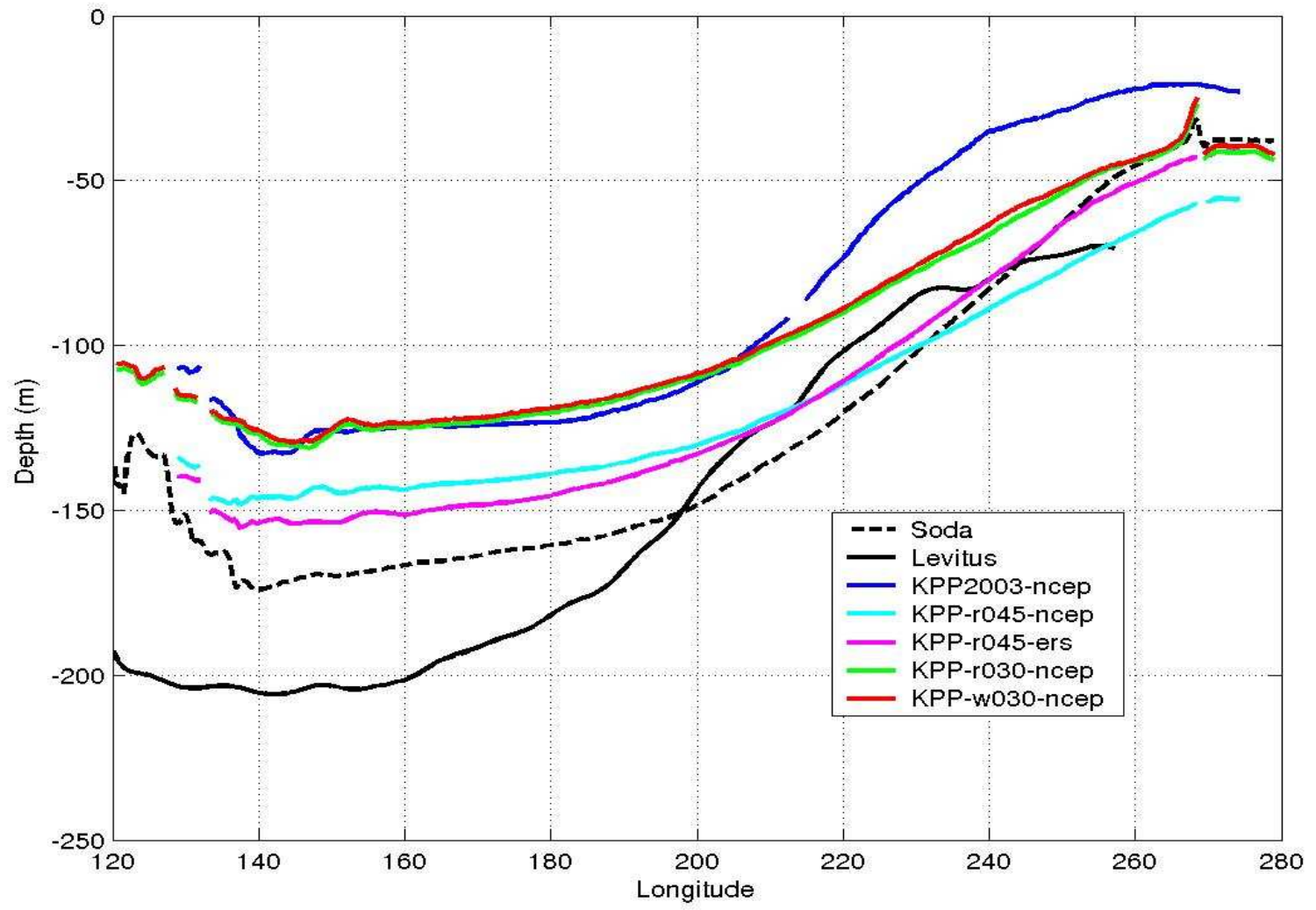


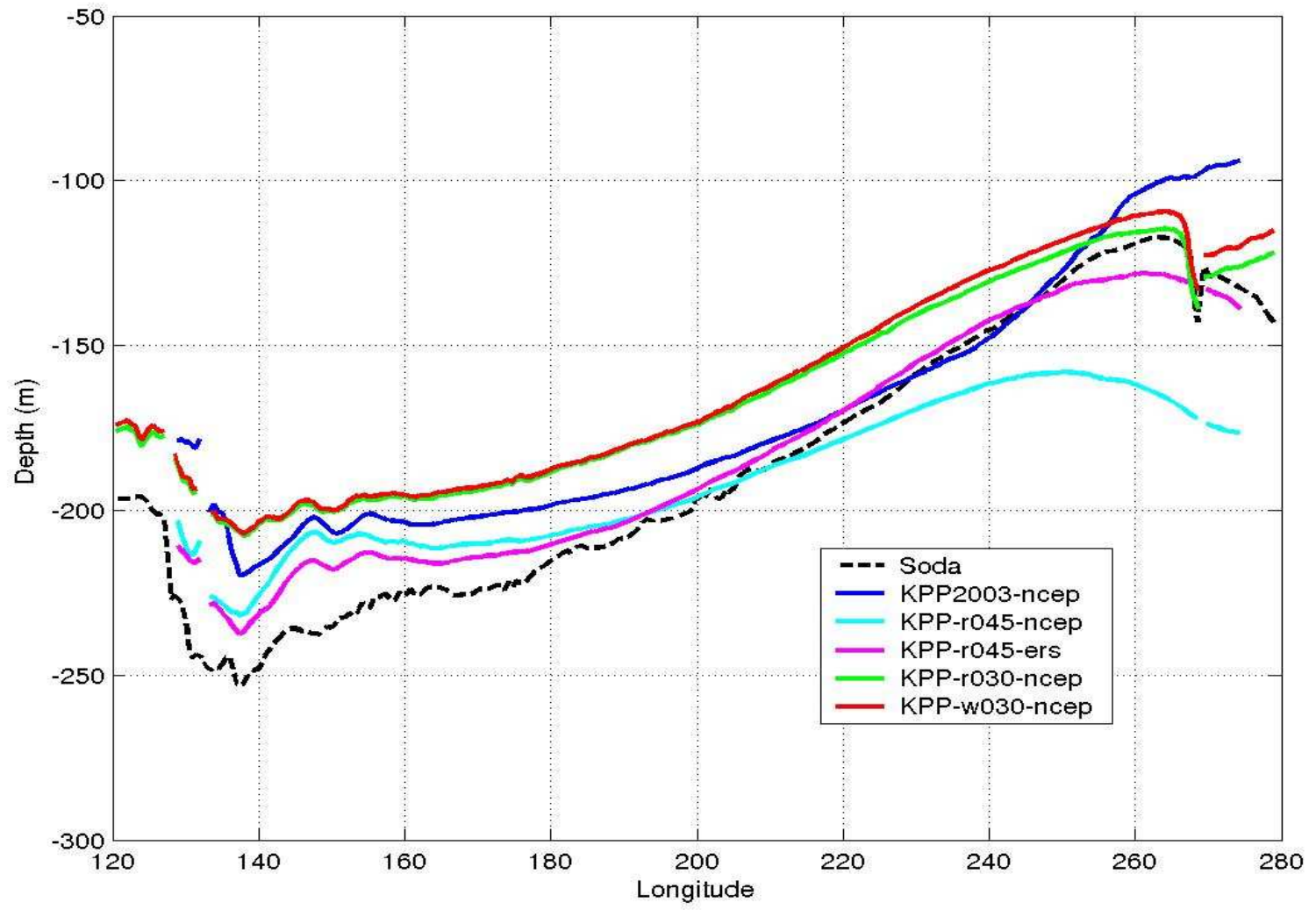
Levitus

vs.



ROMS  
with 2005  
KPP  
still NCEP





## US West Coast Model: an Example of Fine Tuning

US West Coast Model, 15 km resolution forced by COAMPS daily winds

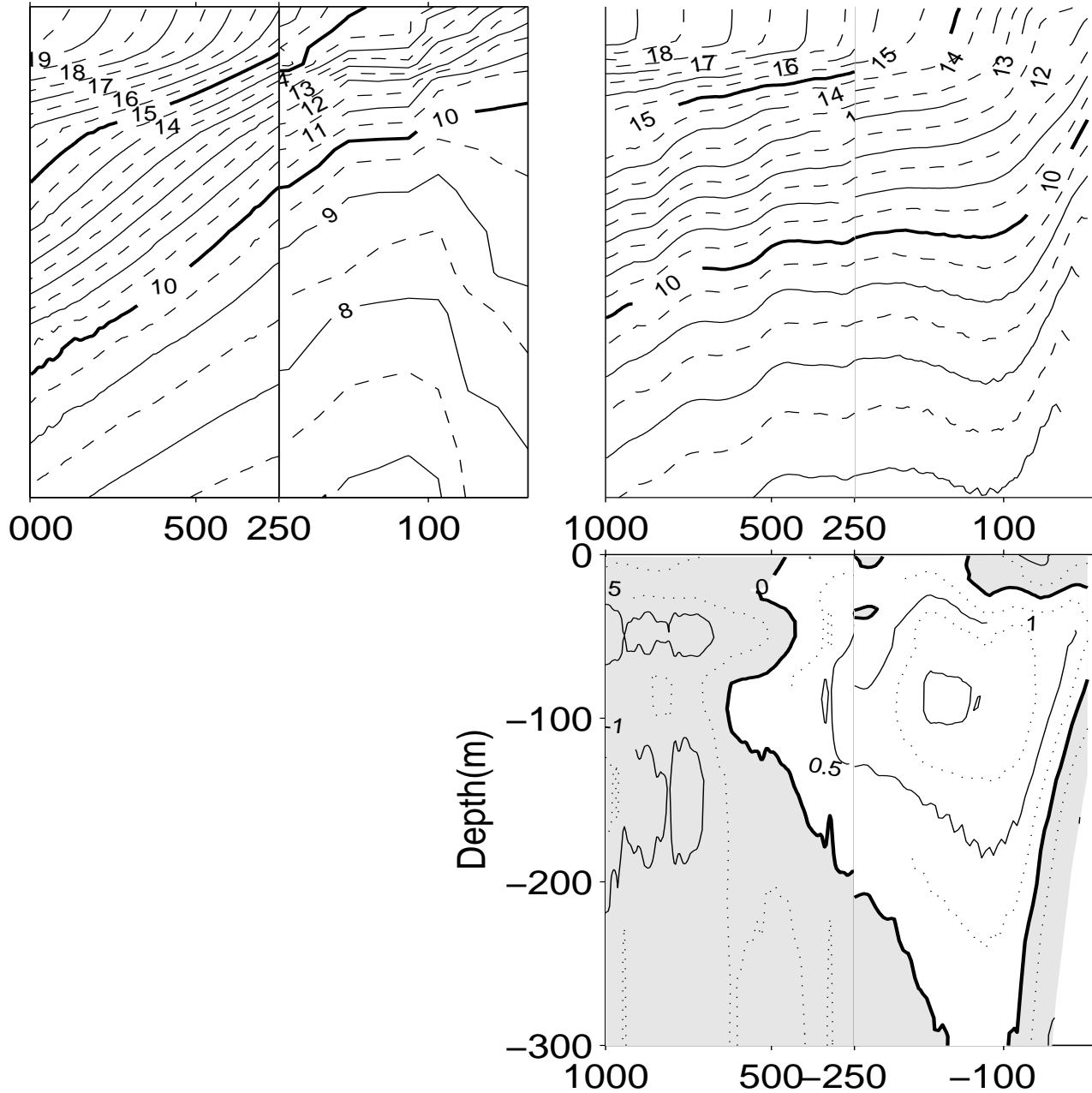
All conditions below are the same, except variations in KPP code.

CalCOFFI (nearshore,  $< 250$  km), and Levitus (beyond that)

showing only summer because this is the worst among 4 seasons

courtesy of Xavier Capet

### S3coamps-daily-15km(sum)



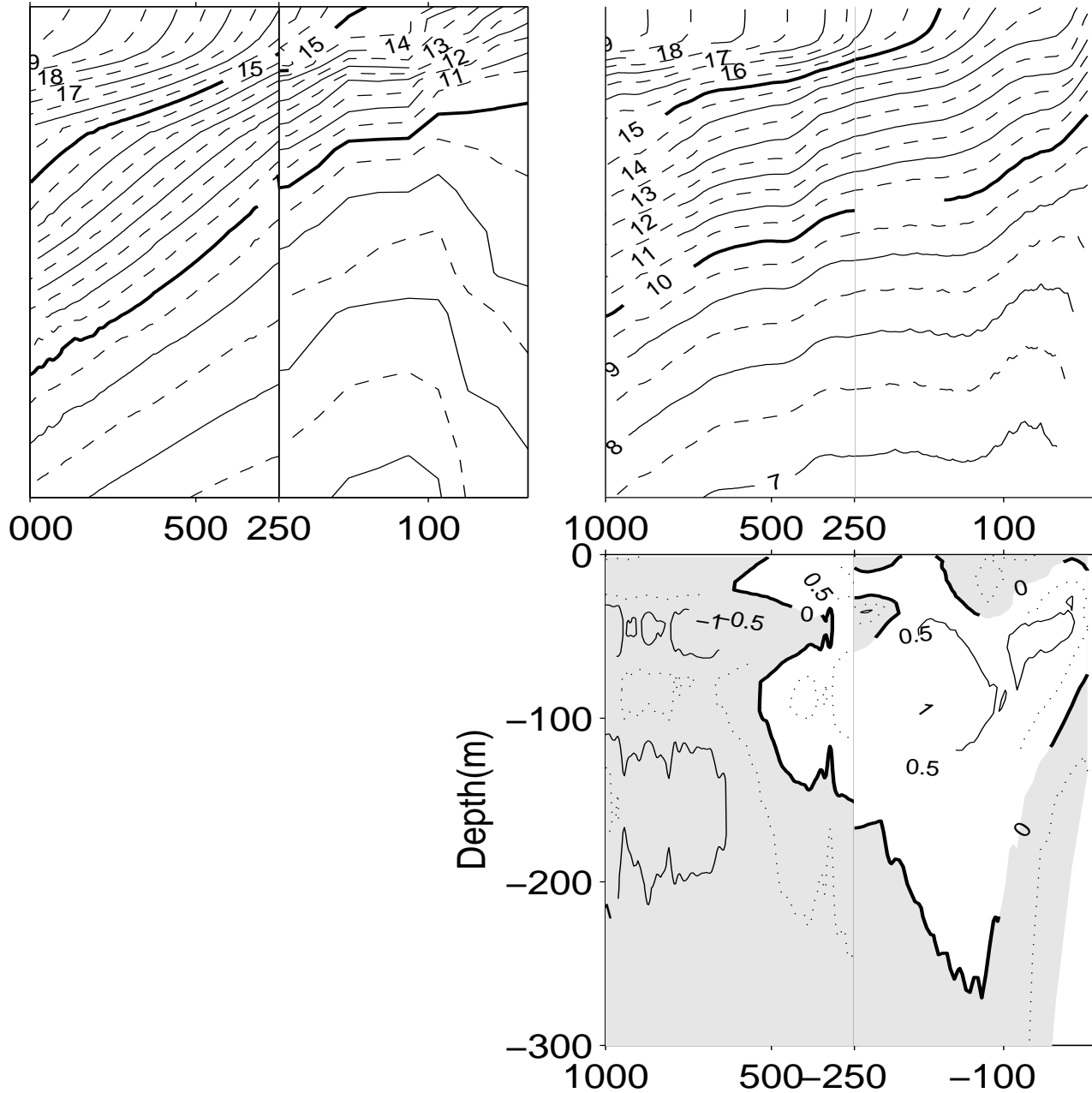
Early 2005 KPP,  
 $Ri_{cr} = 0.45$ , limiting  
 $d/L_{MO}$  for  $w_{m,s}$  in  
 stable regime

Note slope of  
 $10^{\circ}C$ - isotherm

overall  $1.5^{\circ}C$   
 cold bias offshore  
 and  $> 2^{\circ}C$  warm  
 bias nearshore



S3coamps-shallow-15km(sum)



New 2005 KPP

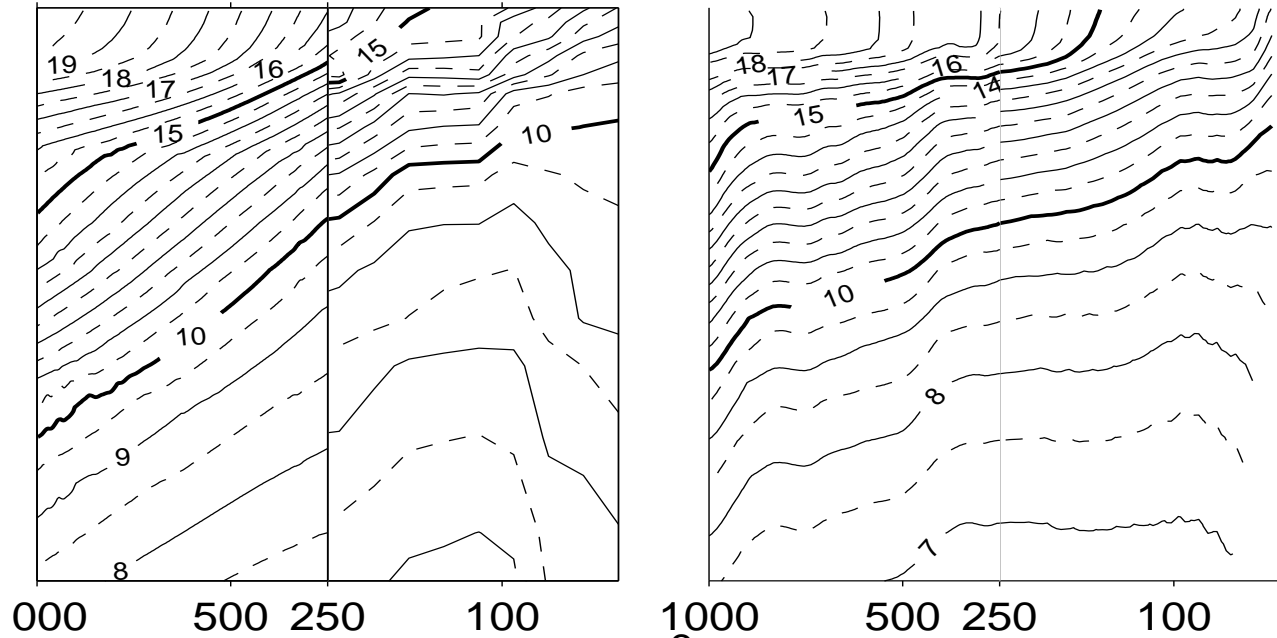
$$Ri_{cr} = 0.45$$

Not limiting  $d/L_{MO}$   
in stable regime

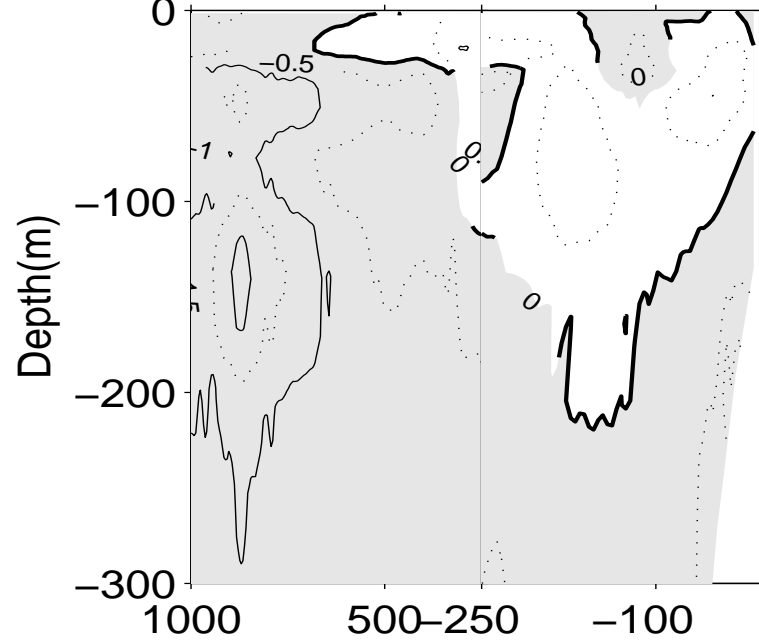
(Fig. 2 of LMD94)

recovered most  
of the slope

# S3coamps-daily\_kkpr-luo-15km(sum)

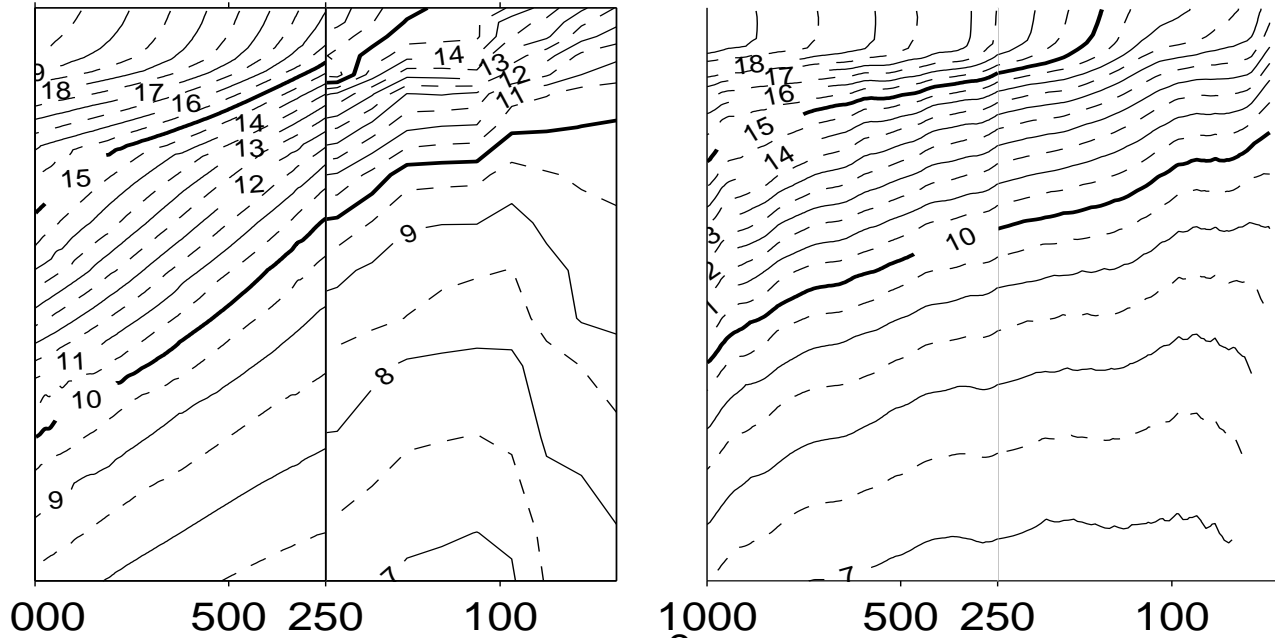


$Ri_{cr} = 0.3$   
No  $d/L_{MO}$  limit

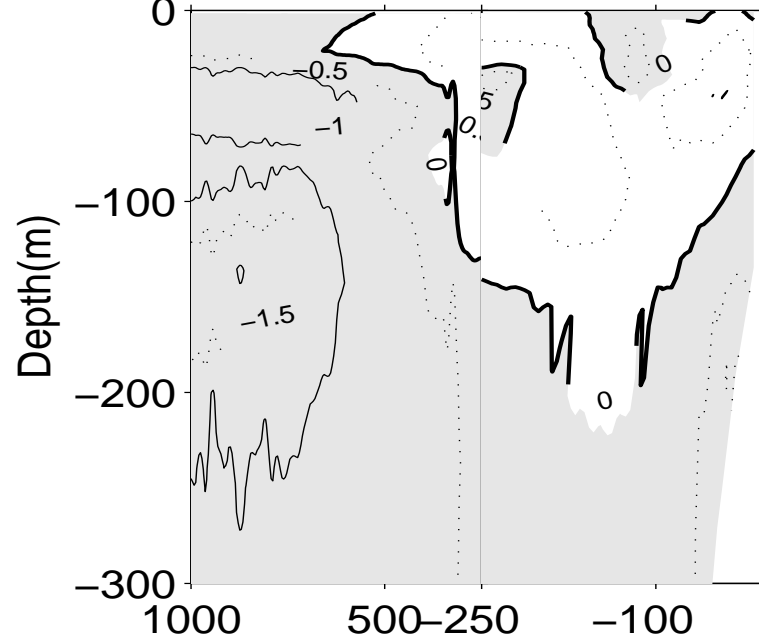


shallow    bias    off-  
shore

S3coamps-daily<sub>n</sub>kkpr-15km(sum)



$Ri_{cr} = 0.3$   
 $d/L_{MO}$  limit



# Summary

- Accepted most (not all) updates from W. Large and G. Danabasoglu
- **integral  $Cr$ -based search for  $h_{bl}$**
- kernel  $\mathcal{K}(\sigma)$  to account for surface sublayer  $\Rightarrow$  convergence
- replaced  $h_{EK}$  limit with new treatment of Ekman boundary layer
- Corrected Monin-Obukhov limitation algorithm.  
Subsequently eliminated it altogether
- Do not limit  $\zeta = d/L_{MO}$  in  $w_{m,s}$  computation in stable regime
- Changed non-local flux to ensure its continuity at  $h_{bl}$
- Surface wave mixing:  $A_k \rightarrow$  finite limit at  $z \rightarrow \zeta$
- **Significantly reduced resolution drift**
- **"shallow bias" is now under control**
- Changes for free-surface compatibility with free surface of ROMS  
(fixed blow-ups in shallow regions)
- code rewritten from scratch (yet, again) for efficiency

## Lessons learned

- 1D model is very useful for process studies and numerical algorithm verification, but **not for parameter tuning against real-world data**
- Boundary layer depth  $h_{bl}$ , as diagnosed by KPP, is not directly comparable to mixed layer empirically derived from data (cf., Levitus,  $0.8^{\circ}$  C-rule, etc). Compare primary field [T,S] field structure instead.
- 3D simulations show significantly less sensitivity to KPP algorithm and parameter settings than 1D, yet the quantitative differences are comparable to that of different forcing products